

平成26年度合同会合
2014.8.1 筑波大学 大学会館

モデリングの現状 トカマクダイバータシミュレーション

星野一生

原子力機構



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1. 国際的進展 (PSI2014概要)

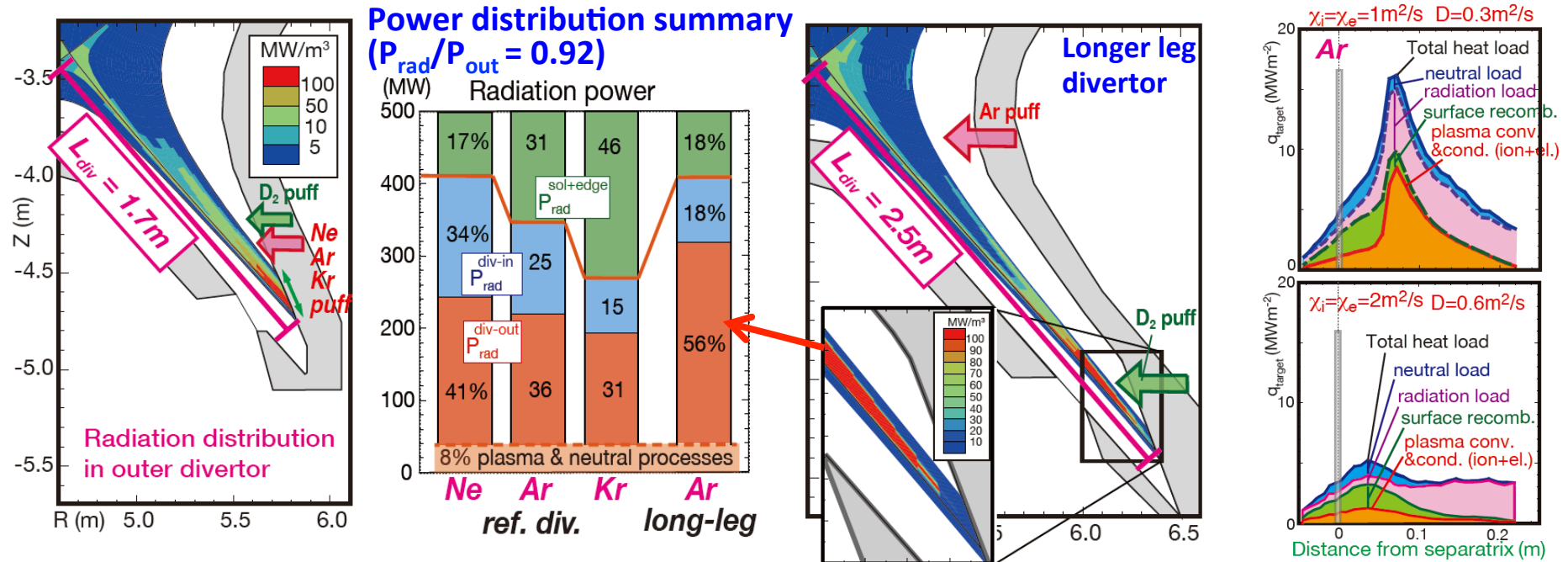
<http://psi2014.nifs.ac.jp/talks.html> を参照してください。

2. 国内活動(原型炉ダイバータシミュレーション)

Power exhaust study for SlimCS ($P_{fus} = 3GW$) in 2012

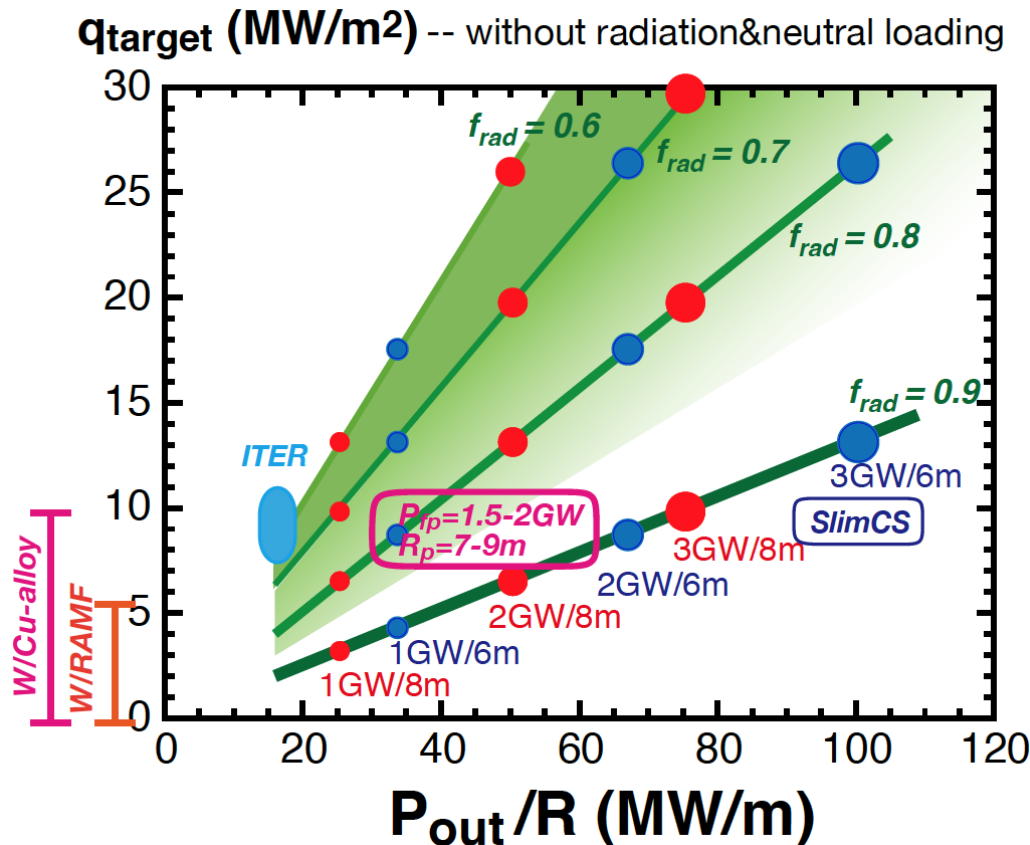
- **Enhancement of P_{rad}^{div} and $P_{rad}^{SOL+edge}$ and “Full detachment”** were required.
 \Rightarrow **Divertor operation consistent with q_{target} (incl. radiation load) $< 10MWm^{-2}$ was seen *only in specific conditions such as enhanced diffusion.***
- **Seeding impurity selection: higher Z (Ar/Kr) is preferable to increase P_{rad}^{SOL}**
 issue: dilution in core plasma, and potentially, P_{rad}^{edge} restriction for good confinement.
- **Longer leg divertor design: effective for full detachment and P_{rad}^{div} enhancement**
 issues: reduction in ion and neutral fluxes, and optimization with He exhaust
- **Plasma diffusion – large impact on detachment and energy dissipation, suggesting that *global/local enhancement promotes full detachment.*** Issues: extrapolation to Demo, techniques.

[1] K. Hoshino, et al. Contrib. Plasma Phys. 52 (2012) 550. [2] N. Asakura, et al. Nucl. Fusion, 53 (2013) 123013.



Demo design for $P_{out}/R = 30-60$ started from 2013

- Design parameters for power exhaust with $P_{out}/R = 30-60$: 2-4 times larger than ITER
 $P_{fus} = 1.5-2GW$ level ($P_{out} = 300-400MW$) and $R = 7-9$ m.
- Large $f_{rad} = 0.8-0.9$ and ITER divertor technology (W&Cu-alloy) will be still required, while experiments with high H-factor and radiation loss are limited up to $f_{rad} = 0.7-0.8$.
 \Rightarrow Developments of the divertor physics and engineering/technology are necessary.



Simple estimation of peak heat load:

$$q_{target} = \frac{P_{out}}{R} \frac{(1 - f_{rad}) \sin q_{div}}{4\pi l_q^{mid} f_{exp_{div}}}$$

$n_e^{SOL\&div}$, Imp. seeding
 Transport & Detachment
 Geometry design
 Divertor physics design study will decrease q_{target} in Figure.

Nearly full-detachment was obtained in reduced P_{fus}

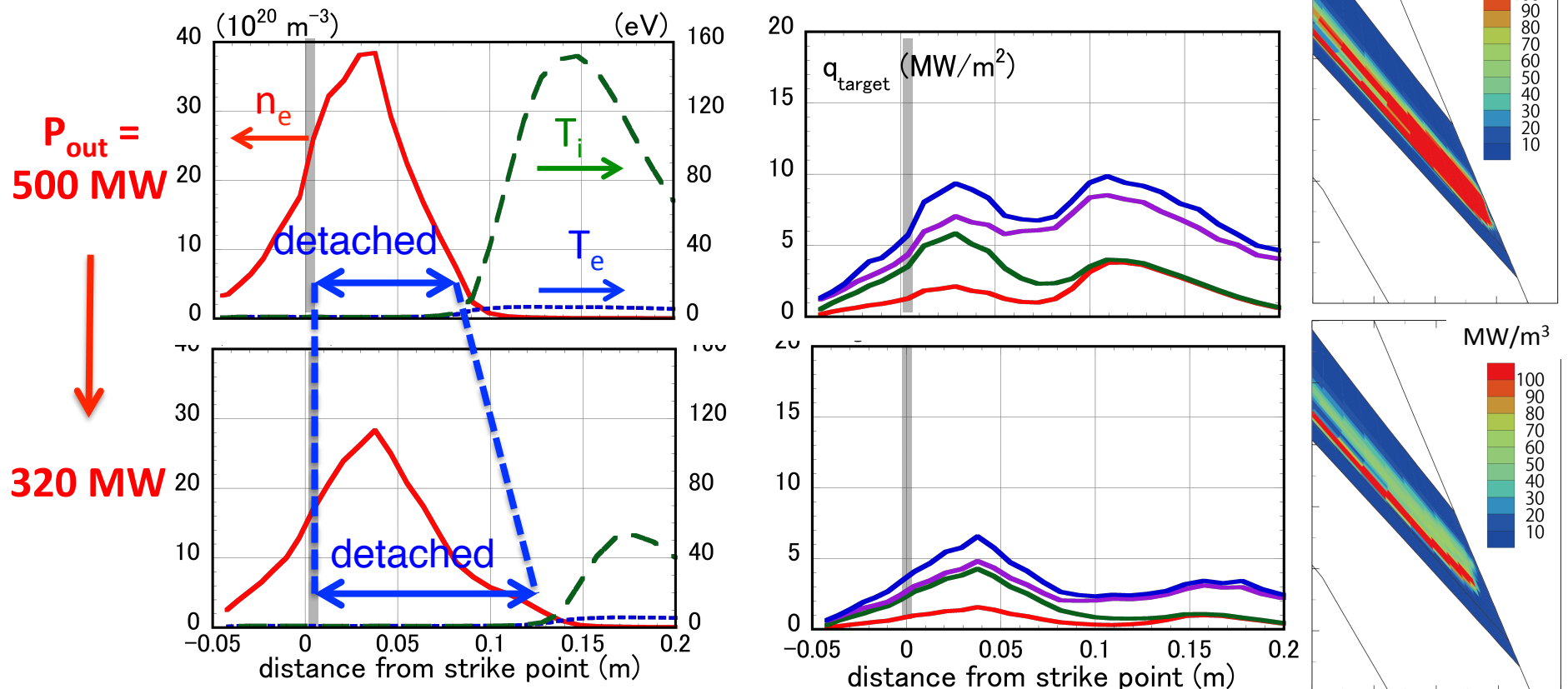
$P_{out} = 500 \Rightarrow 320\text{MW}$ (P_{fus} decreases from 3GW to 2 GW)

SONIC solution of $f_{rad} \sim 92\%$ ($P_{rad}=295\text{MW}$) was obtained by Ar puff of $10\text{ Pa/m}^3\text{s}$

Impurity radiation moves upstream \Rightarrow detached region further extends to 12cm.

\Rightarrow The peak heat load decreases to 6MW/m^2 .

Note: thermal instability at the divertor will be investigated in future.



Divertor operation ($< 10\text{MWm}^{-2}$) is expected at $f_{\text{rad}} > 80\%$

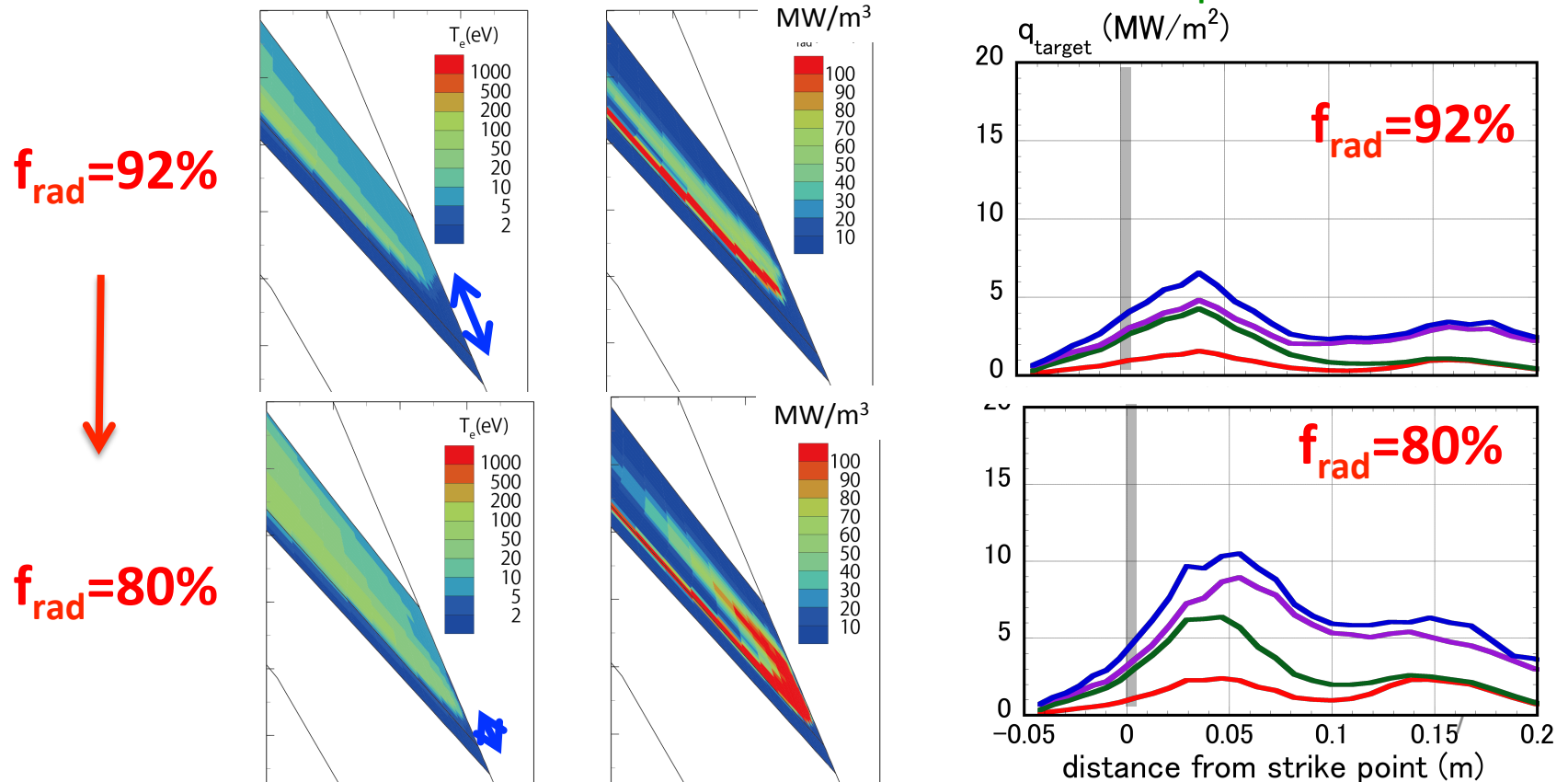
Radiation region moves near target with reduction from $f_{\text{rad}} = 92\%$ ($P_{\text{rad}}^{\text{tot}} = 295\text{MW}$) to 80% (256MW), where nearly full-detached plasma becomes partially-detached.

⇒ Peak heat load increases from 6 to 10MW/m^2 .

Lower $f_{\text{rad}} < 80\%$ seems to be difficult in the SlimCS-size divertor.

Studies in 2014:

- Impurity (Ne/Ar/Kr) seeding and long-leg option will be compared to $P_{\text{fus}} = 3\text{GW}$.
- Divertor operation in similar geometry for New concept design ($R_p \sim 8\text{m}$)



Divertor simulation of new design: $R_p \sim 8\text{m}$, $P_{\text{out}} = 320\text{ MW}$

SONIC simulation of the divertor plasma in the new Demo design with reduced P_{fus} : large radiation loss case ($f_{\text{rad}}=92\%$) showed that full detached was enhanced.

\Rightarrow thermal instability of the divertor plasma occurs.

Calculations of lower radiation cases ($f_{\text{rad}} = 70\text{-}85\%$) are now in progress.

Input parameters are the same

At core boundary $r/a \sim 0.95$:

Exhausted power from core P_{out} is given

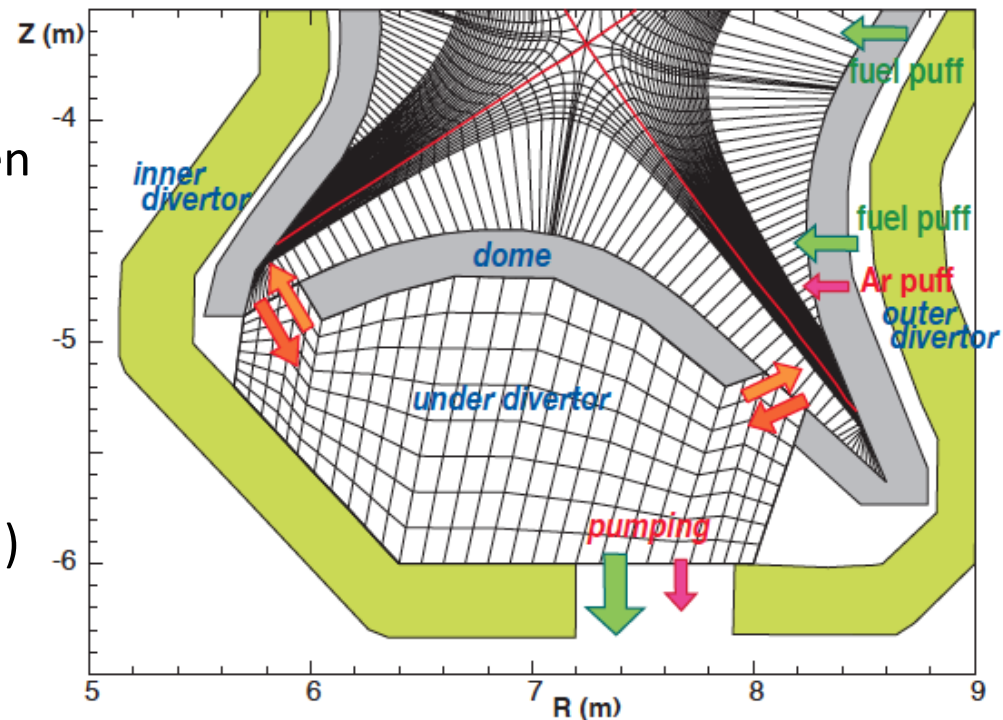
$$n_{D^+} = 7.0 \times 10^{19} \text{ m}^{-3}$$

Transport coeff. (same as ITER calc.):

$$D = 0.3 \text{ m}^2/\text{s}, \quad c = 1.0 \text{ m}^2/\text{s}$$

D gas puff: $G_{\text{puff}} = 0.8 \times 10^{23} \text{ s}^{-1}$ (div. + sol)

pumping speed: $S_{\text{pump}} = 200 \text{ m}^3/\text{s}$



3. 日欧共同研究

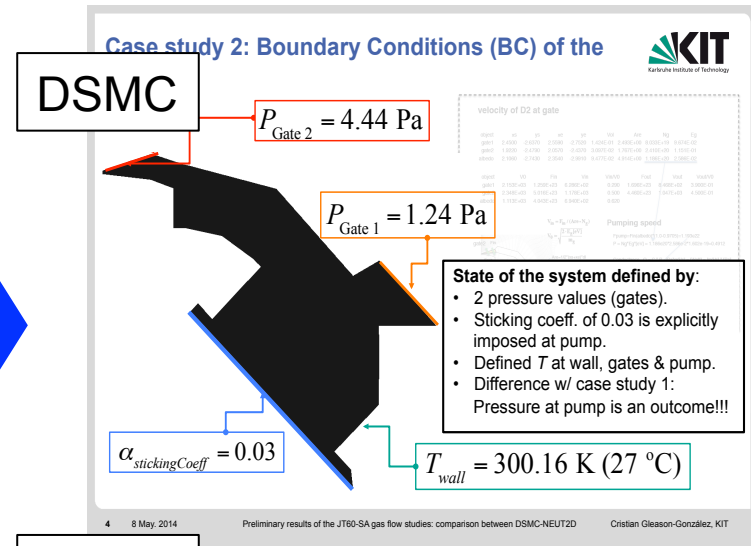
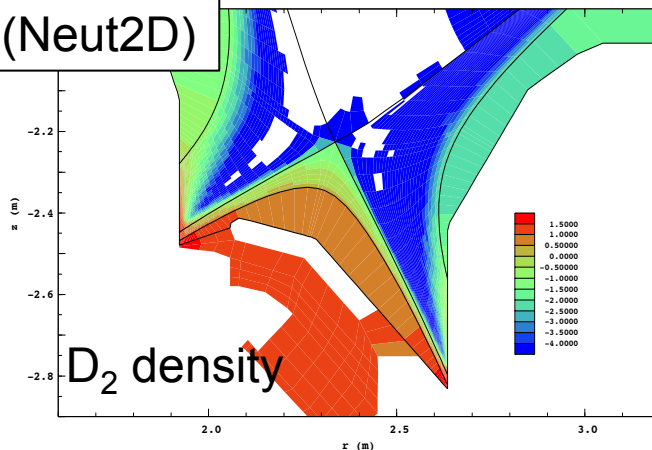
Comparison DSMC and NEUT2D for subdivertor gas flows in JT60-SA

Kick-off meeting at JET on 22/3/2014

C. Gleason-González, S. Varoutis, K. Hoshino, H. Utoh, N. Asakura, T. Nakano

Boundary conditions defined and given:

SONIC (Neut2D)



2nd meeting (remote) on 8/5/2014

C. Gleason-González, S. Varoutis, K. Hoshino,

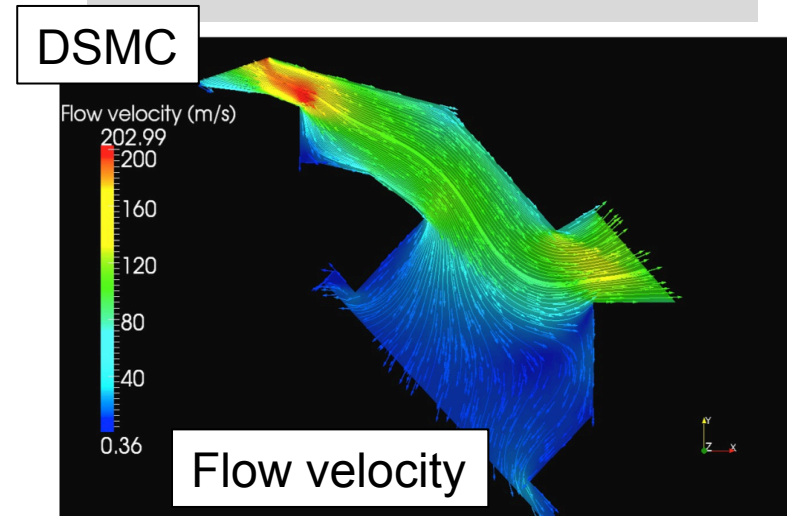
K. Shimizu, S. Sakurai, N. Asakura, T. Nakano

1st output from DSMC code:

Some difference found

The boundary conditions are being checked

Simplified calculation model was suggested



JET modelling by SONIC

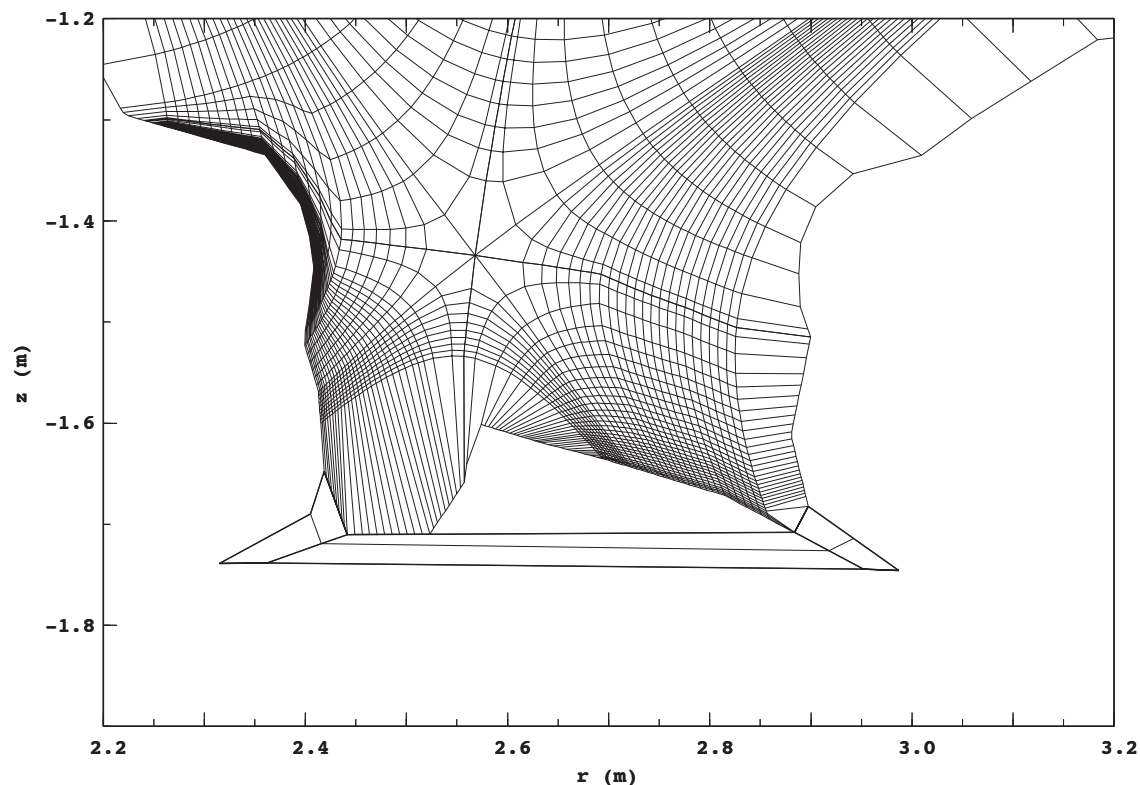
デタッチメントモデリングの改善を目標に、今年からコード間ベンチマークを再開

(cf. ITPA DSOL mtg. 2009)

すでにSOLPSやEDGE2Dで解析の進んでいる**JET-ILW**を対象に、
SONICシミュレーションに着手

初期結果について、10月の
ITPA(DSOL)で報告予定

SONIC mesh for JET-ILW



まとめ

1. 国際的進展

実験データを補完的に用いた解析が精力的に進められている。実験データの再現性は高くなってきているが、unconventional assumptionによるところが大きいと思われ、今後モデリングが必要。

2. 国内活動

原型炉ダイバータとしては、原型炉仕様の再検討を受け、パラメータサーベイを開始。課題はあるものの $2\text{GW } P_{\text{rad}}/P_{\text{out}}=92\%$ で現状の工学設計と取り合える可能性が見えてきた。

JT-60SAの解析については、燃料・不純物ガスの組み合わせを変えたようなパラメータサーベイが進行中。またW壁の解析も始められている。

3. 日欧共同研究

サブダイバータの中性粒子輸送、デタッチメントモデル改善に向けたコード間ベンチマークが進行中