

EMC3-EIRENEによる 周辺プラズマ・不純物輸送モデリング

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◆ EMC3-EIRENEによる周辺プラズマモデリング

- ◆ LHDにおける周辺プラズマ解析
- ◆ タングステンダイバータ損耗再堆積解析
- ◆ 直線装置プラズマモデリング

Transport simulation of LHD peripheral plasmas

Background and Motivations

- Understandings of plasma-neutralimpurity interactions and realization of predictive simulation.
- Evaluation of different divertor configuration; open and closed.
- Approach
 - Realization of three-dimensional transport simulation in ergodic and leg regions in the realistic geometry.
 - Development of a three-dimensional transport code for LHD; EMC3 EIRENE
 - Validation by measurements.
 - Comparisons of results for open/closed divertor configurations.





- EMC3 solves fluid equations of flux tube plasma in SOL: $\nabla_{\parallel} \cdot (n\mathbf{v}_{\parallel}) + \nabla_{\perp} \cdot (-D\nabla_{\perp}n) = S_{p}$ $\nabla_{\parallel} \cdot (m_{i}n\mathbf{v}_{\parallel}\mathbf{v}_{\parallel} - \eta_{\parallel}\nabla_{\parallel}\mathbf{v}_{\parallel}) + \nabla_{\perp} \cdot (-m_{i}\mathbf{v}_{\parallel}D\nabla_{\perp}n - \eta_{\perp}\nabla_{\perp}\mathbf{v}_{\parallel}) = \nabla_{\parallel}p + \mathbf{S}_{m}$ $\nabla_{\parallel} \cdot \left(-\kappa_{i}\nabla_{\parallel}T_{i} + \frac{5}{2}nT_{i}\mathbf{v}_{\parallel}\right) + \nabla_{\perp} \cdot \left(-\chi_{i}n\nabla_{\perp}T_{i} - \frac{5}{2}T_{i}D\nabla_{\perp}n\right) = k(T_{e} - T_{i}) + S_{ei}$ $\nabla_{\parallel} \cdot \left(-\kappa_{e}\nabla_{\parallel}T_{e} + \frac{5}{2}nT_{e}\mathbf{v}_{\parallel}\right) + \nabla_{\perp} \cdot \left(-\chi_{e}n\nabla_{\perp}T_{e} - \frac{5}{2}T_{e}D\nabla_{\perp}n\right) = -k(T_{e} - T_{i}) + S_{ee}$
- EMC3 can simulate plasma with ergodic magnetic field in LHD by solving them with the aid of Monte Carlo method.





- 18°-section (1/20 of the torus) is realized in simulation by using the periodicity and assumption of up-down symmetry.
- Meshes are generated on poloidal planes every 0.25°.





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- Conditions and Assumptions
 - Input power: 8MW
 - Electron density: 2×10¹³/cm³ at LCFS
 - Bohm condition is assumed at divertor plates
 - Magnetic configuration: R_{ax}=3.6m
 - Perpendicular transport coefficient: $D_{perp}=1 \text{ m}^2/\text{s}$, $\chi_{perp}=3 \text{ m}^2/\text{s}$
 - No neutral-pumping (100% recycled)





- Influence of the closed configuration on neutral-gas pressure
 - Compression of hydrogen gas
 - Simulation gives 17 times higher density under the dome structure.
 - It agrees with experimental measurement (10~20 times)



Scaling of neutral pressure with electron density

- A series of simulation were carried out.
 - Constant input power: 8MW, n_e at LCFS: 1, 2, 4,6, 8×10¹³/cm³.
- Dependence of neutral pressure on electron density.
 - Simulation results has the same scaling law as the experimental measurements independently of configurations.



Comparison of neutral pressure; measurements of two discharges and simulation results (solid lines: 500K H₂ gas)



- Recycling in open/closed configuration
 - Closed configuration causes large particle source, i.e. large recycling.
 - Large ionization leads to large energy loss.
- Contribution of divertor legs on recycling
 - Major contribution in low-density discharges, 1~4×10¹³/cm³
 - Minor contribution in high-density discharges, 6~8×10¹³/cm³





Impurity screening [M. Kobayashi et al., JNM 390 (2009) 325] $\begin{cases} Friction force \propto w_{\parallel} \rightarrow divertor plates \\ Thermal force \propto \nabla_{\parallel}T_{e} \rightarrow core \end{cases}$





 Friction force vs. thermal force

thermal force dominant

toward the upstream



friction force dominant toward the downstream





- Assumptions for qualitative comparison
 - Sputtering yield is fixed to 1%.
 - Self sputtering is not included.
 - Sputtered carbon is treated as an atom.
- Large recycling flux leads to large erosion.
- Modification to the closed configuration causes large erosion.
- Amount of the generation \neq Accumulation in the plasma



Impurity retention in the plasma

- Total carbon amount, i.e. $[C^+]+[C^{2+}]+...+[C^{6+}]$
 - Leg regions
 - Impurity retention increase according to the electron density.
 - Ergodic region
 - Screening effect of the plasma flow significantly reduces the retention in the ergodic region.
 - No influence of configurations is observed in the case of high-density discharges. — Why?





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- Monte Carlo simulation code of erosion and redeposition
- Background plasma distribution is fixed in simulation.
- Code modification to use EMC3-EIRENE results is on going.





EMC3-EIRENE results of heat load on divertor tiles.

- Global estimation of erosion.
- Influence of plasma parameters on the pattern.





- Background plasma from EMC3-EIRENE
- How poloidal/toroidal plasma-distribution affects deposition/erosion of W.



W measurement in LHD

NIES

 A W-coated tile is installed. W-deposition only in the private side Other tiles are made of CFC. erosion x10²⁰ ensity [W/m² 0.6 0.4 dominant R20 W-coated 0.2 100 120 60 80 140 tiles Reference position [mm] x10²⁰ E 1.0 R18 wetted area 0.1 0. 0.2 80 100 120 140 Reference position [mm] E 1.0 1.0 R16 coated tile 0.6 0.4 0.2 40 60 80 140 160 20 100 120 Reference position [mm] wide deposition x10² [_w/M] 0.8 distribution **R8** ≧ 0.6 0.4 0.2 80 100 120 140 160 180 20 [M. Tokitani] 19 Reference position [mm]



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Simulation modeling of linear device

 Linear devices for divertor simulation and PWI H. Tanaka, M. Kobayashi, G. Kawamura (NIFS) N. Ohno, T. Kuwabara, M. Urakawa (Nagoya Univ.) Y. Feng (Max-Planck IPP)

- GAMMA10, NAGDIS-II, MAGNUM-PSI, PISCES-B, PILOT-PSI, PSI-2, JULE-PSI etc.
- Divertor-plasma codes have been developed for tokamak/helical devices.
 - 2D: B2-EIRENE (SOLPS), EDGE2D-NIMBUS, UEDGE-DEGAS2
 - 3D: EMC3-EIRENE
- Simulation of linear device has been reported but relatively new and challenging issue.
 - B2-EIRENE
 - Cylindrical plasma and device
- Advantage of EMC3-EIRNE code
 - 3D geometry of plasma and walls can be simulated.
 - Realistic geometry without cylindrical assumption.





Linear Device for PSI and detachment





Development is in progress.



Summary of the recent progress

- EMC3-EIRENE code and calculation mesh have been extended to LHD with the closed divertor configuration.
- A validation by neutral gas pressure
 - Influence of dome structure in closed configuration was analyzed.
 - The scaling of neutral pressure to n_e(LCFS) is in good agreement.
- Impurity screening effect in the open/closed configuration.
 - Screening effect due to the flow is recovered in the ergodic region.
 - Increase of impurity generation in the closed configuration.
- Application to ERO simulation
- Modeling of a linear device



- Neutral particles
 - Pumping under the dome, wall pumping, gas-puffing
 - Penetration to the core (TASK3D)
- Impurities
 - Divertor configuration
 - Transport related to screening
- PWI
 - Local simulation at LHD W tile (ERO)
 - Global erosion estimation
- Measurements
 - Transport coefficient modeling from Thomson scattering
 - 2D imaging of impurity radiation
- Detachment
 - LHD (impurity seeding, RMP)
 - NAGDIS-II (1D)