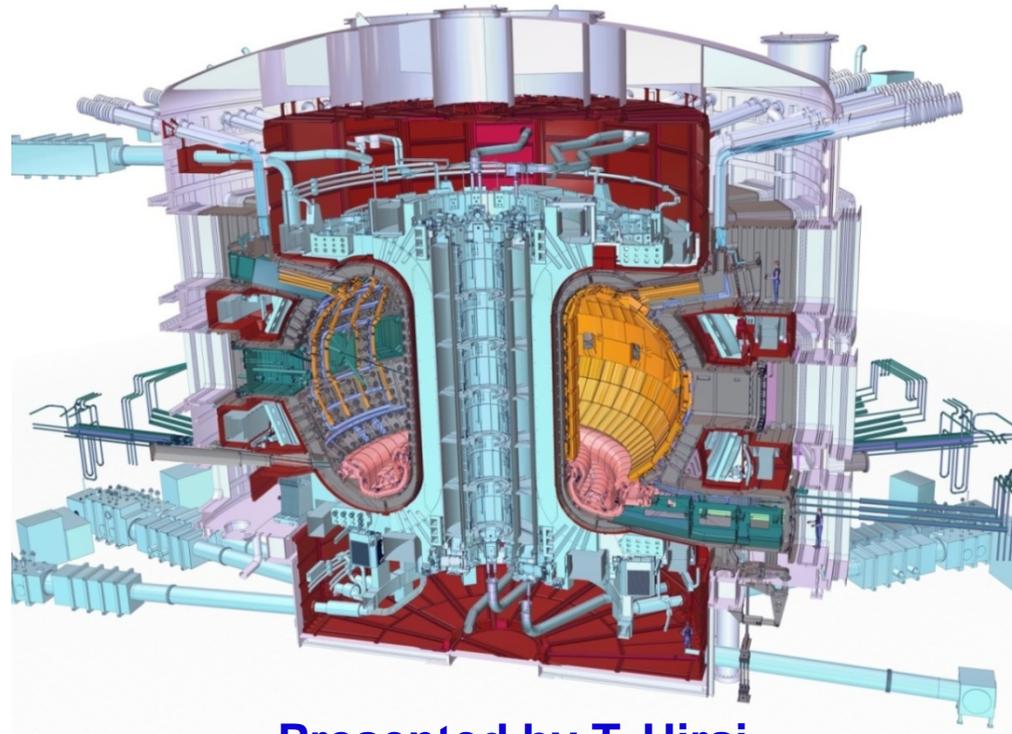


ITER full W Divertor Design and Progress of Technology R&D



Presented by T. Hirai

Tungsten Divertor Section, ITER Organization
On behalf of Tungsten Divertor Task Force at IO

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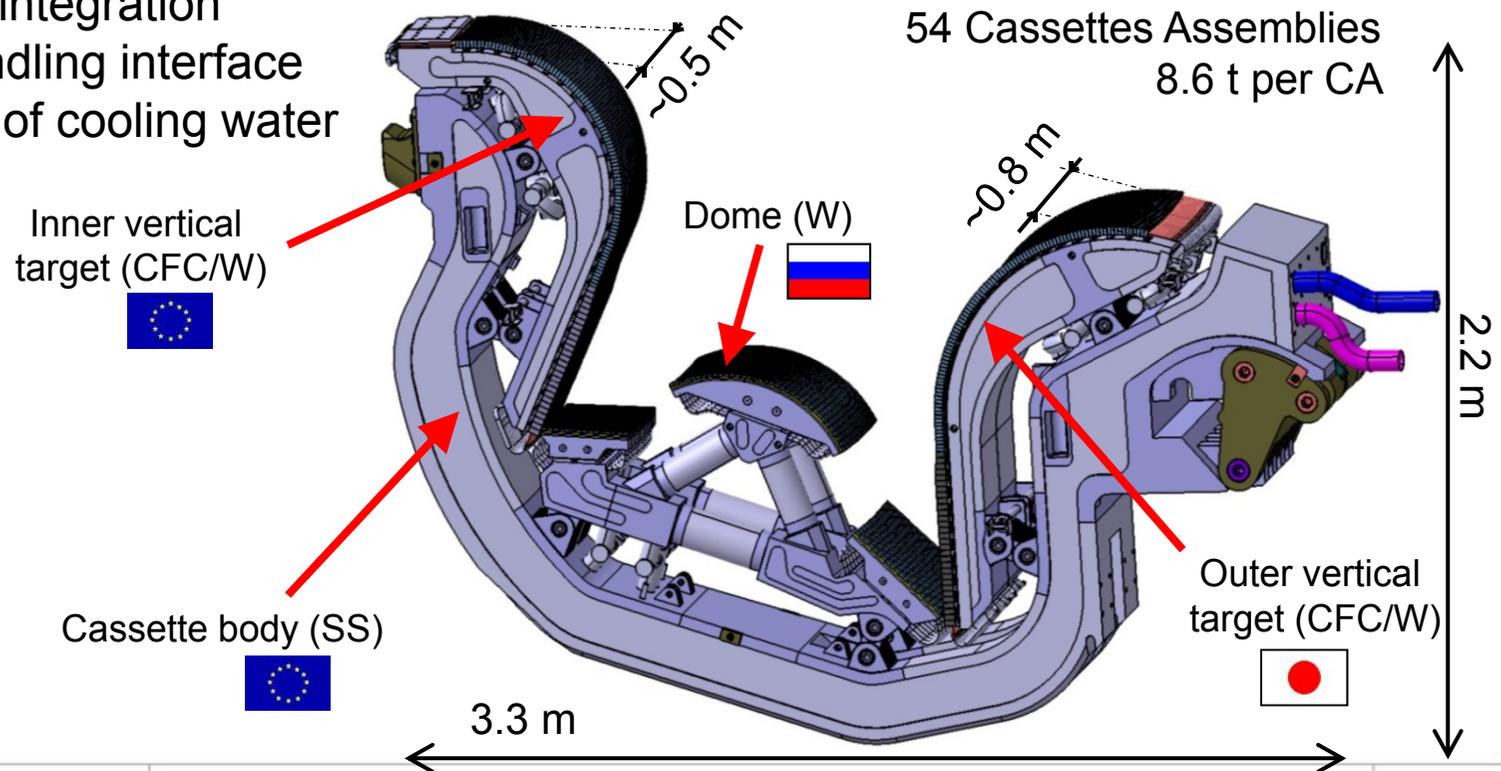
W. Shu

M. Sugihara

*** TF leader**

Divertor Cassette assembly

1. 54 Divertor Cassettes + 6 spare Cassettes
2. 3 Plasma-Facing Components (PFCs) on a cassette
3. Outer/Inner **Vertical Targets, Dome** (Umbrella and Reflector Plates)
4. Plasma-Facing Units (**monoblock** for VT PFUs and **flat tile** concept for Dome PFUs)
5. Plasma-facing Unit Attachments (plug and support leg)
6. Plasma-facing Component Attachments (Pin and multilink)
7. Divertor Cassette Attachments (Nose and Knuckle)
8. Diagnostics integration
9. Remote Handling interface
10. Circulation of cooling water



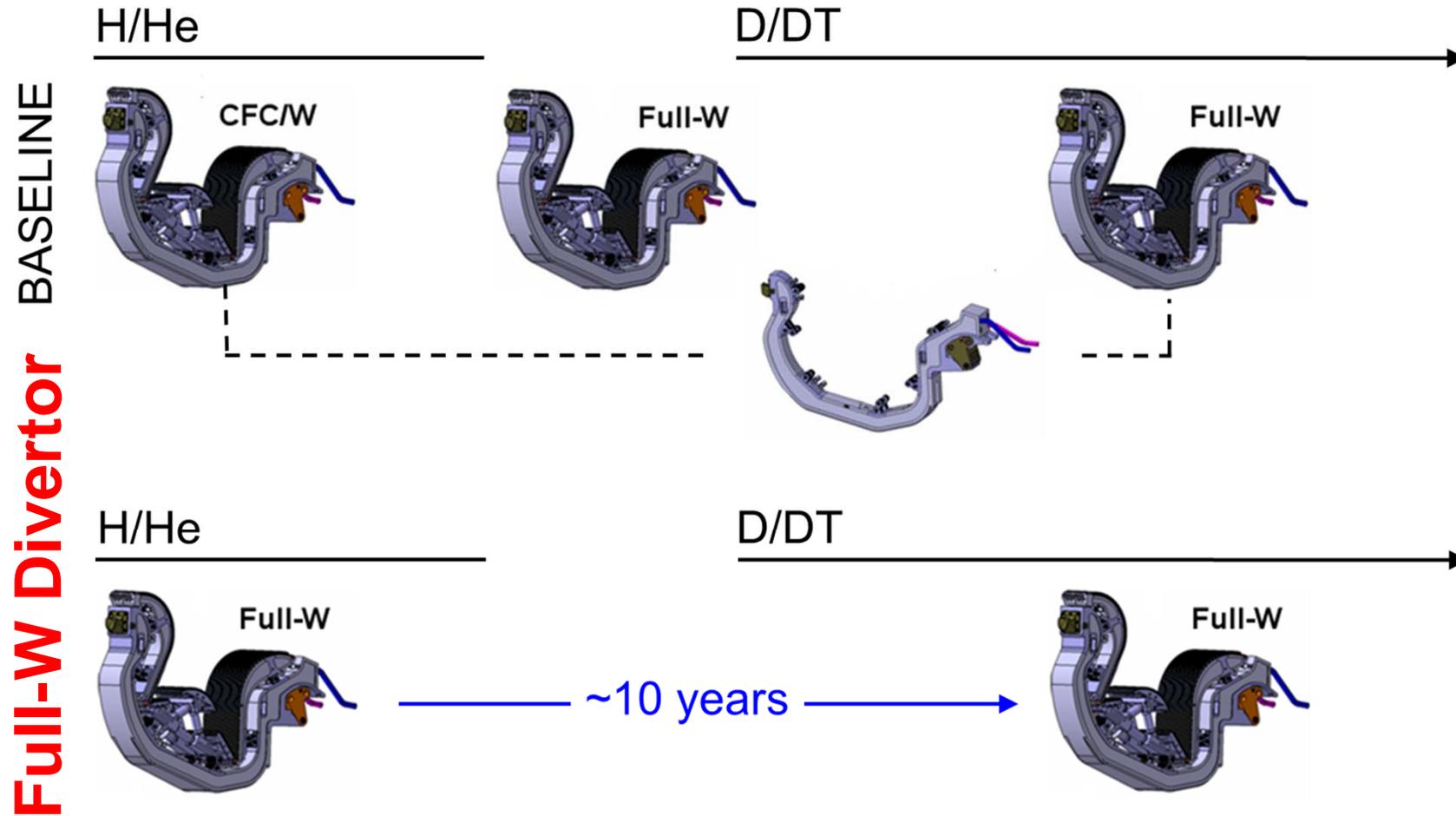
Background of Full-W Divertor Activity

- **New ITER divertor strategy**

- From MAC-12 (Oct. 2011) [ITER_D_6SR5F7]: “[...] for budgeting purposes, the MAC supports the DG recommendation to de-scope to a single divertor during construction and initial five years of operation”.[...] “As to the specific choice of divertor, MAC recommends delaying the decision for up to two years.
- These recommendations were adopted by the ITER Council during its ninth meeting in Nov. 2011 so that IO started to investigate the possibility of beginning operation with a full-W armoured divertor.

Divertor Maintenance strategy

- Extension of Lifetime



Outline

- 1. Design constrain/input**
2. Detailed divertor PFC Design
3. Design Validation
4. Technology R&D requirements
5. Progress of technology R&D in EU and JA
6. Conclusion/Schedule

W Divertor Design – Requirements/ Input

- **Structural Design**

- Load Specification for the ITER Divertor ([C9RF33](#))
- Structural Design Criteria – In-vessel Component (SDC-IC) ([222QGL](#))

- **Plasma-Facing Unit Design**

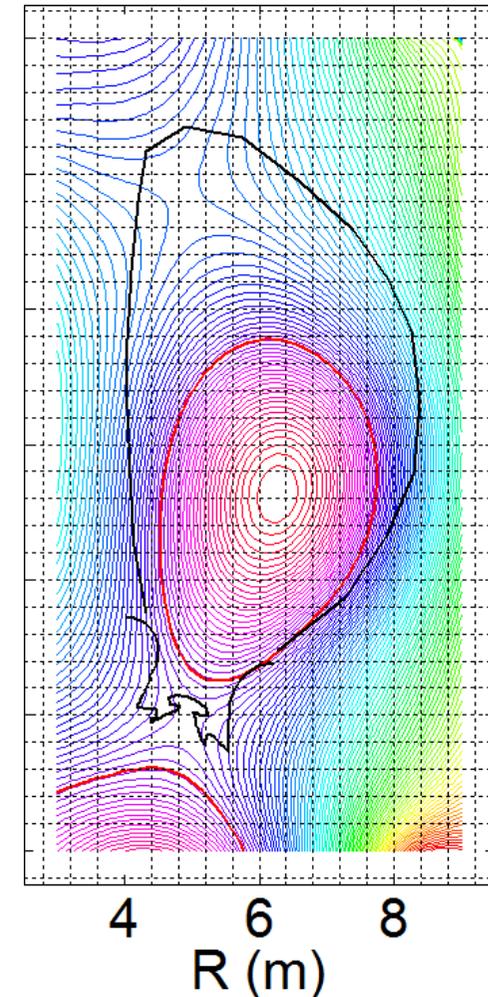
- Heat Load Specification for ITER Tungsten Divertor:
 - (1) Power density and number of cycles on the Vertical Target ([7GFMB6](#))
 - (2) Poloidal conductive/convective surface heat loads ([HDB7NZ](#))

- **Tolerances**

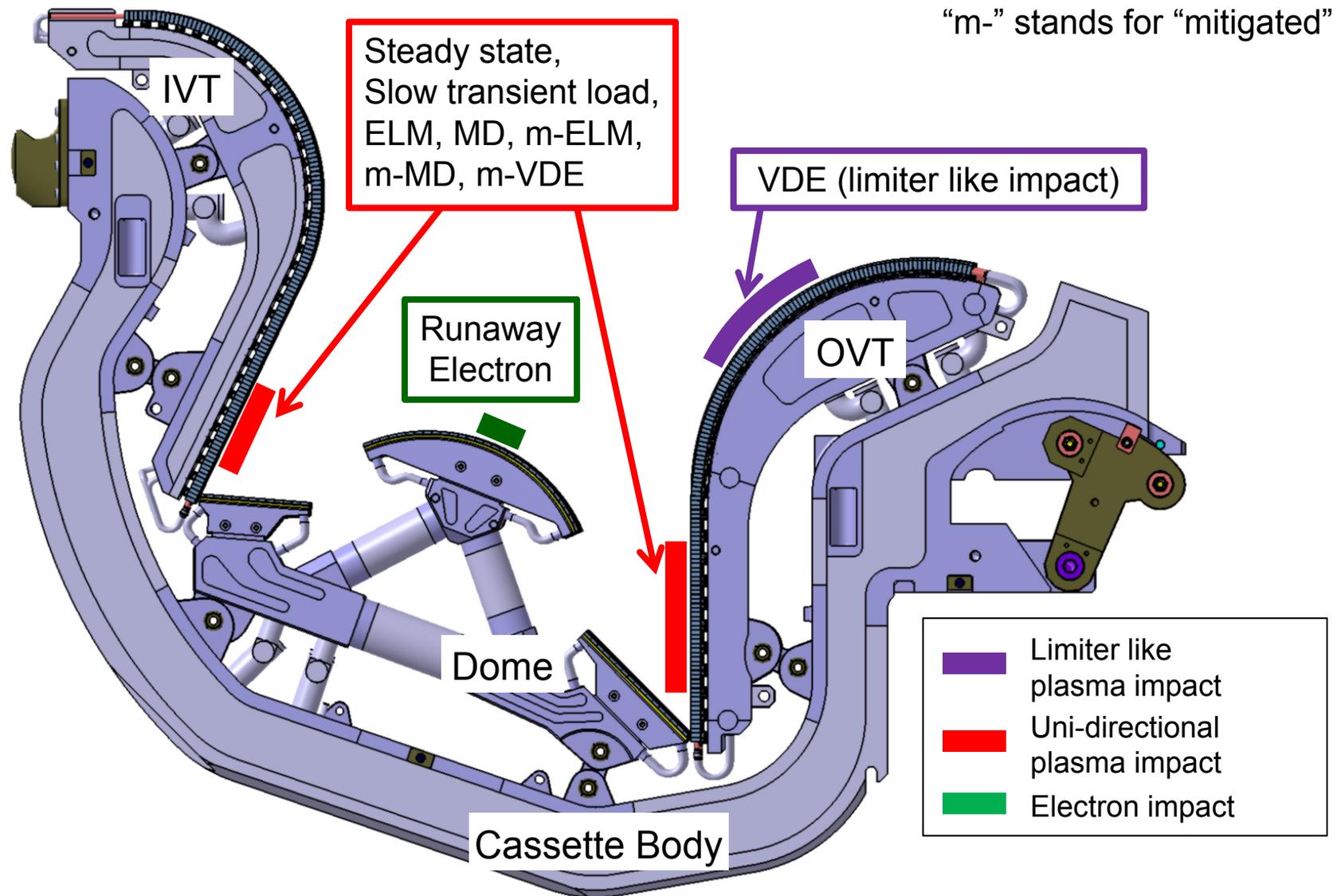
- Assembly tolerances between Cassettes (20mm gap) : **step ± 2 mm** (*Divertor Plasma Facing Surfaces Position and Shadowing Tolerances Build Up (764MGY), and margin*)
- Assembly tolerances between two halves of VT PFCs (3mm gap) : **step ± 0.3 mm** (*in 2D drawings*)
- Assembly tolerances between VT PFUs (0.5mm gap): **step ± 0.3 mm** (*in 2D drawings*)

W Divertor Design: Design Constrains/ Assumptions

1. **Single coolant tube** for a PFU to limit impact on CB design, diagnostics procurement, assembly plan, other interfaces (splitting target and baffle is not considered)
2. **Dome design is retained** as long as neutronics analysis confirms
3. **Materials for Tungsten Divertor remain same** except (a) exchange of CFC by W and (b) updated radioprotection requirements
4. **Monoblock concept is retained**
5. PFU attachment concept (PFU to the steel support structure) is retained.
6. **DW VDE (limiter configuration) contact only at OVT baffle** according to the recent DINA analysis (ITER_D_765S86).



Thermal Event Impact at Plasma-Facing Surfaces



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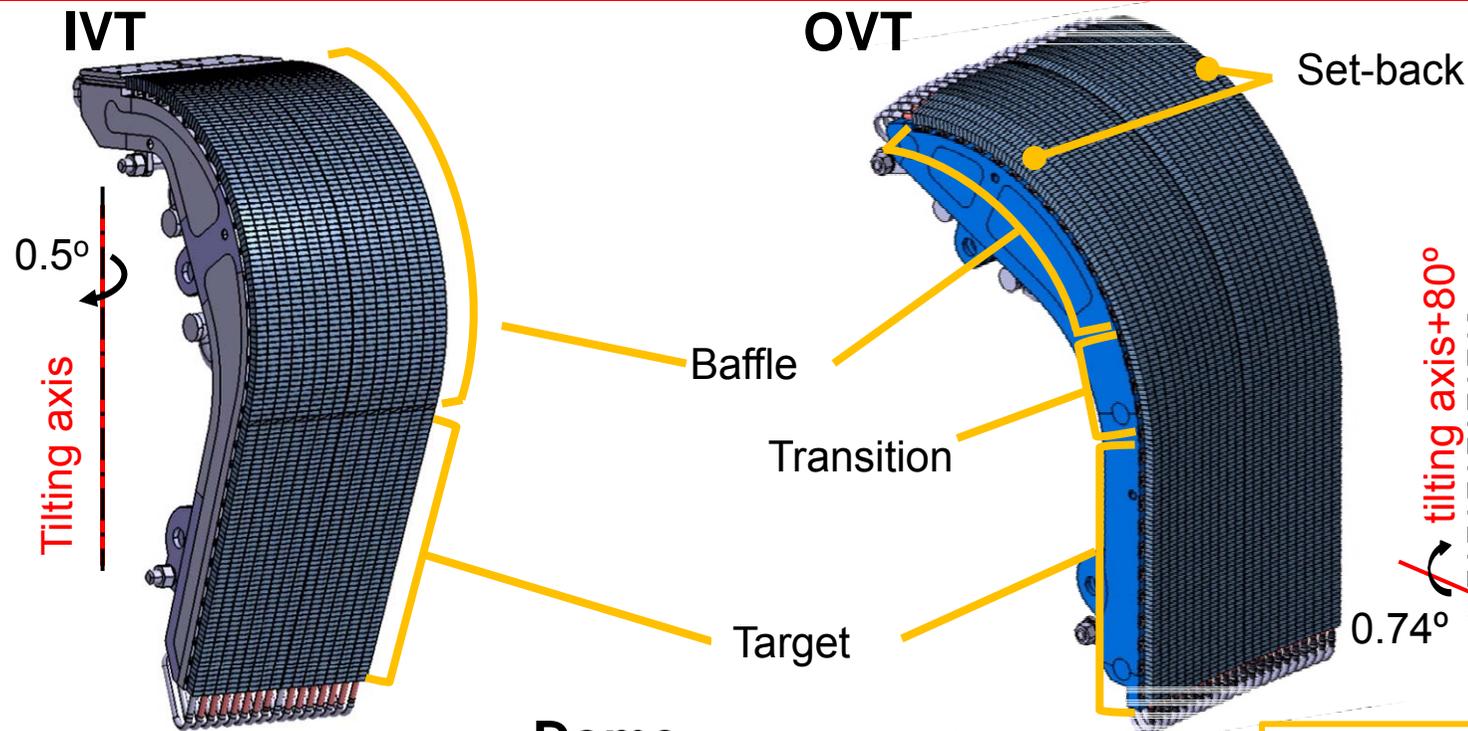
Divertor Shaping Strategy

Objective:

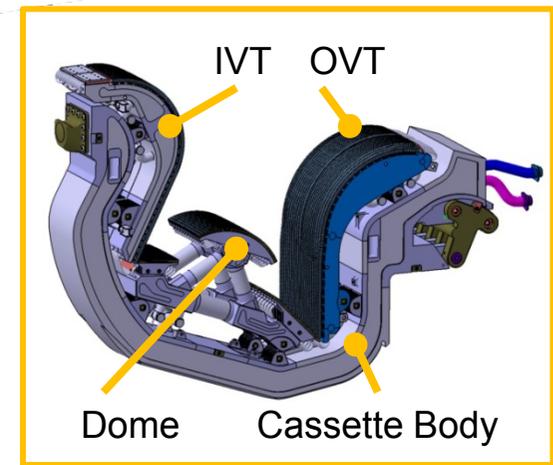
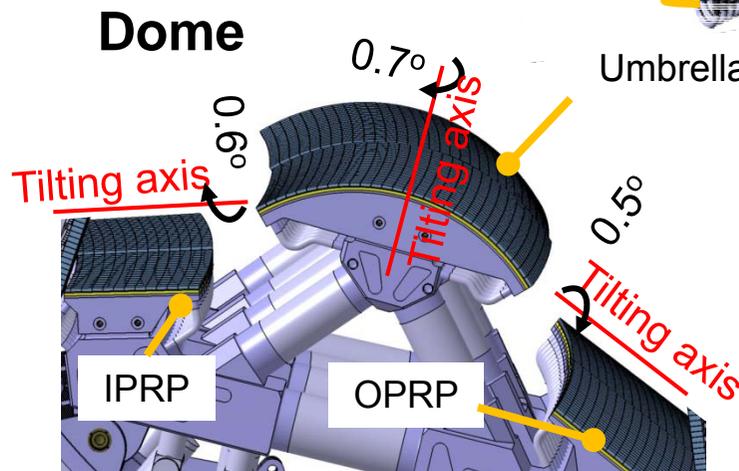
To avoid melting due to leading edge exposure during steady-state and slow transient and to minimize the melting under off-normal events –
full edge-shadowing in high heat flux handling areas

1. Tilting of each Divertor Plasma-Facing Component
2. Toroidal-Roof-shaping and Outer Vertical Target chamfer
3. Monoblock toroidal chamfer

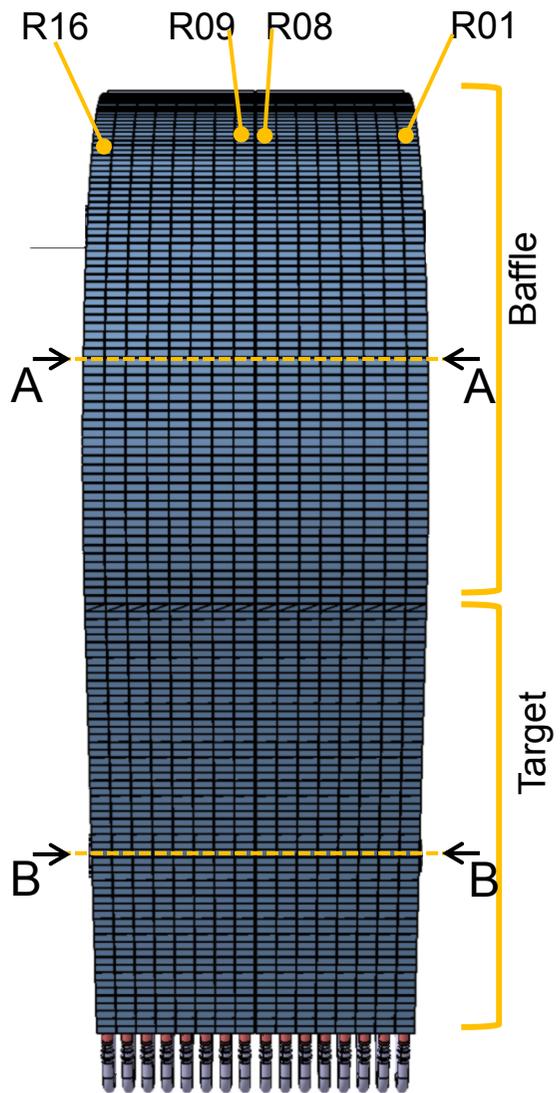
Tilting Scheme for OVT, IVT and Dome



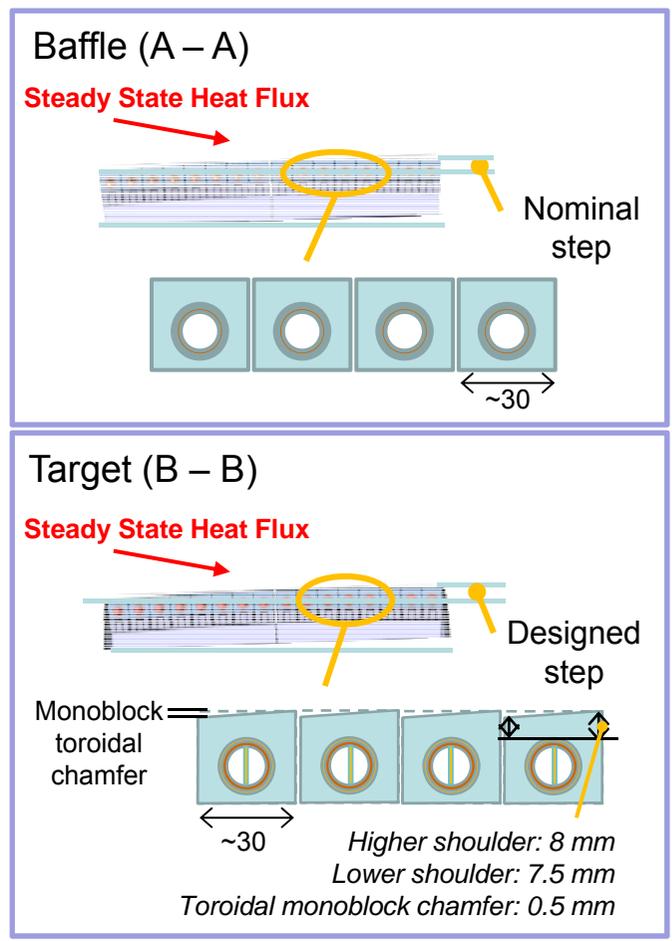
Tilting - By tilting of OVT and IVT, a **nominal step** between VT is implemented at the strike point regions. Components are tilted when assembled onto the Cassette Body (CB), to ensure no W leading edges from PFC to PFC



IVT design – Monoblock toroidal chamfer at target



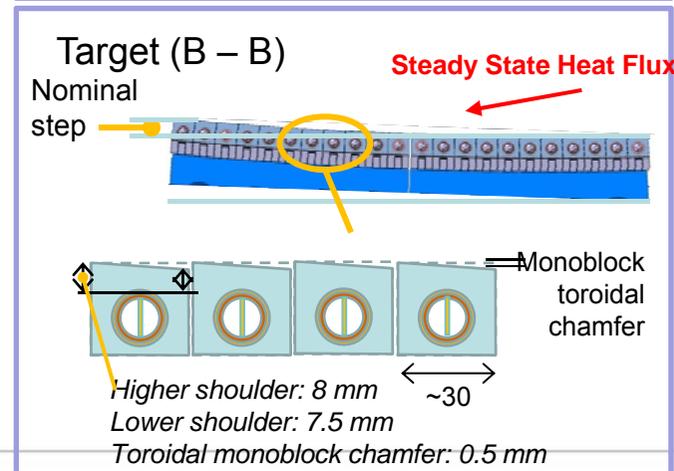
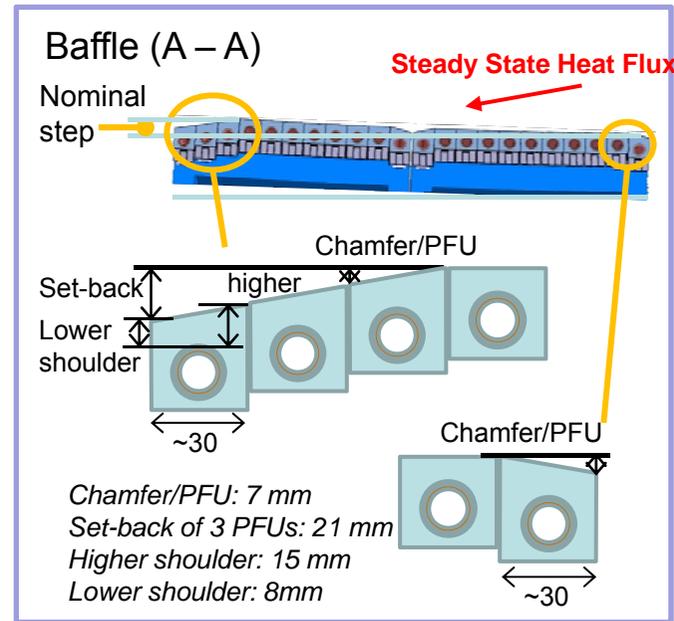
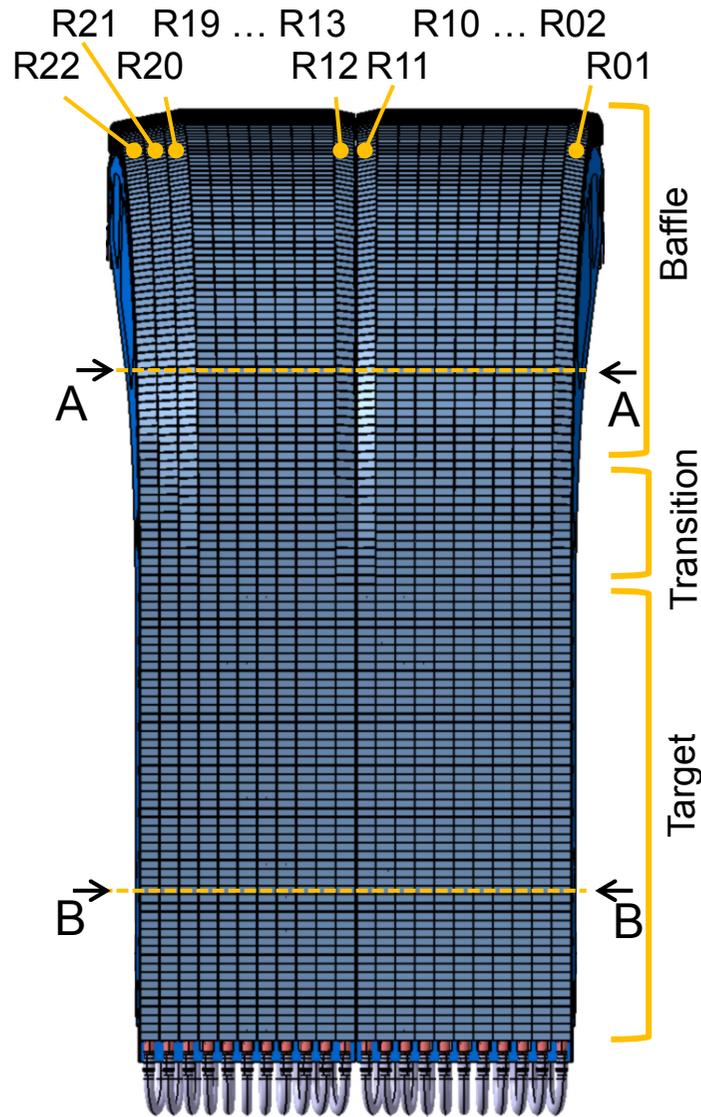
PFU variant: R01=R02...R16 (Reference PFUs)



Monoblock toroidal chamfer to protect edge from 0.3 mm deviation → 0.5 mm toroidal monoblock chamfer

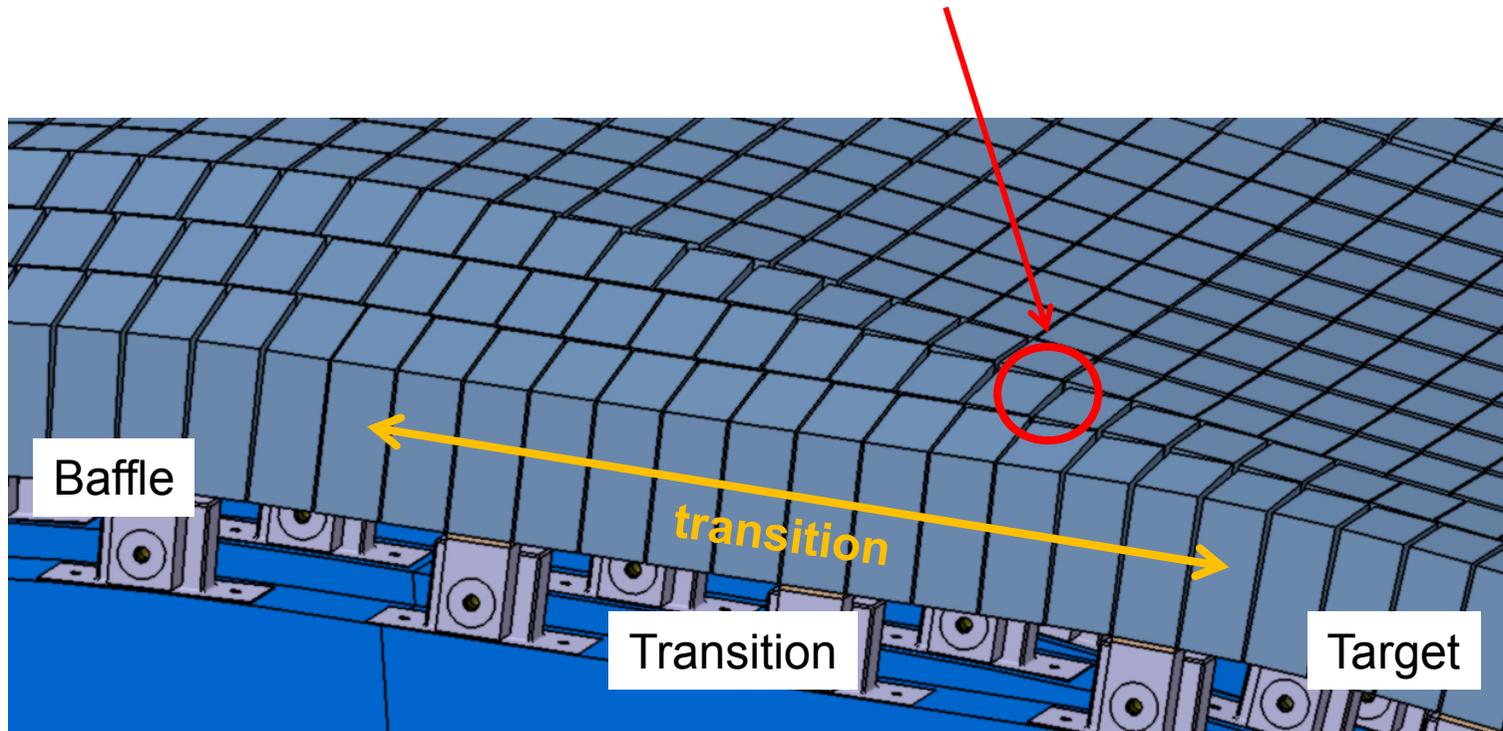
OVT design: PFC chamfer + monoblock chamfer

PFU variants: R01=R12; R11=R20;
R02= R03...R10, R13...R19 (reference PFUs)



OVT design – Transition from target to baffle

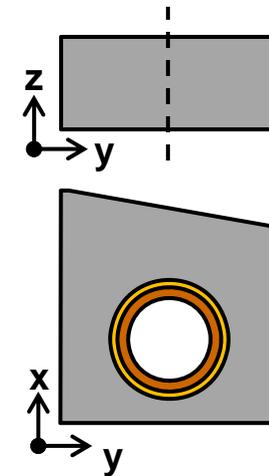
- **Transition: (1) monoblock thickness; (2) monoblock toroidal chamfer; (3) PFU profile**
 - Monoblocks have simple chamfers at plasma facing side
 - Location of transition: away from the VDE impact area – steady state loading area
 - Poloidal edge: exposed toward bottom direction



Manufacturing of W monoblock and PFU

• W Monoblock

- Monoblocks consist of simple chamfer or double chamfer at plasma facing side (No complicated 3D profile)
- Monoblocks can be manufactured by conventional operations such as:
 - EDM wire cut operation (no need of milling)
 - Grinding operation
 - Conventional cleaning process
- Inspection i.e. dimension control, to be defined in NDT protocol



• PFU

- **OVT: only 5 variants**

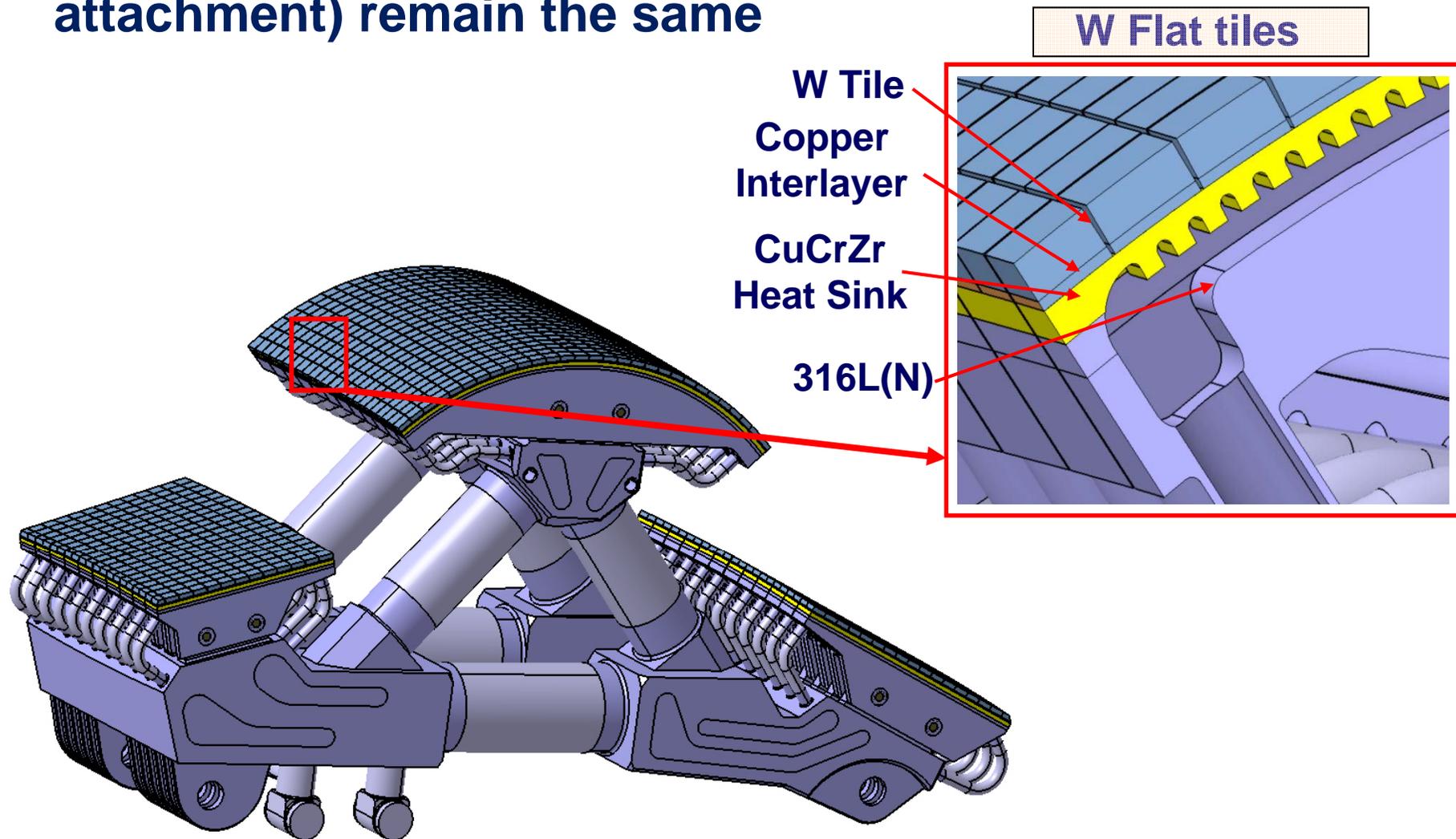
Reference OVT PFU $R2 = R3-R10 = R13-R19$;

Toroidal roof shaping OVT PFUs $R1=R12$; $R11=R20$; $R21$; $R22$

- **IVT: only 1 variant**

Dome cooling structure and PFU attachment

- Dome design (cooling structure & PFU attachment) remain the same



Outline

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Design Validation by analysis

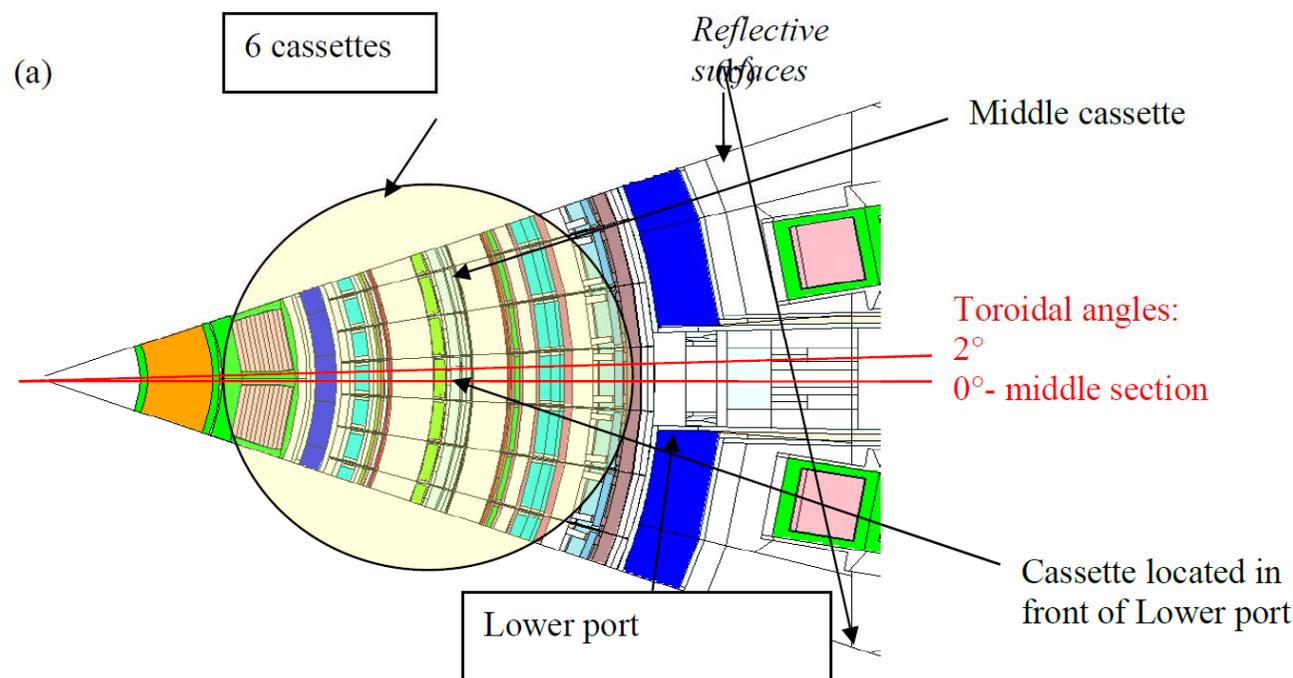
1. Neutronic analysis
2. Design Supporting analysis (thermo-mechanical and EM analysis)
3. Heat Load distribution Study – PFC and monoblock level

Nuclear Analysis for ITER W Divertor

Model: Neutronic analysis by means of the latest ITER MCNP-5 Monte Carlo Code for 3D model (MCNP ITER 40° model B-lite v-2)

Assumption: 18% of the cumulated 3×10^{27} neutrons (End of Life) during first divertor (up to end of the first full DT campaign)

Aim: Evaluate nuclear heating, radiation damage and helium production



Nuclear Analysis Results – damage (dpa)

Villari - Neutronic Analysis (ITER_D_HQZHC5)

Maximum dpa at ITER EOL (permanent)			
Component	W	Cu/CuCrZr	SS
IVT PFU	0.51	2.37	1.28
OVT PFU	0.54	2.50	1.52
Dome Umbrella PFU	0.48	2.11	1.31
CB plate below Dome			0.14
Maximum dpa after 4 years of ITER nuclear phase (first cassette)			
Component	W	Cu/CuCrZr	SS
IVT PFU	0.089	0.41	0.22
OVT PFU	0.095	0.44	0.27
Dome Umbrella PFU	0.084	0.37	0.23
CB plate below Dome			0.025

Design supporting analysis

Input:

Defined Load combinations in Load Specification for the ITER Divertor (C9RF33)

Aim:

Validate structural integrity under the following loads and load combinations by FEM

- Inertial loads (associated with gravity and seismic events);
- Hydraulic pressure loads,
- Electromagnetic loads,
- Thermal loads (due to nuclear heating and surface heat fluxes), and
- Assembly loads (typically due to preloads imposed on the CB during assembly and preload of the bolts).

Design supporting analysis – Load Combinations

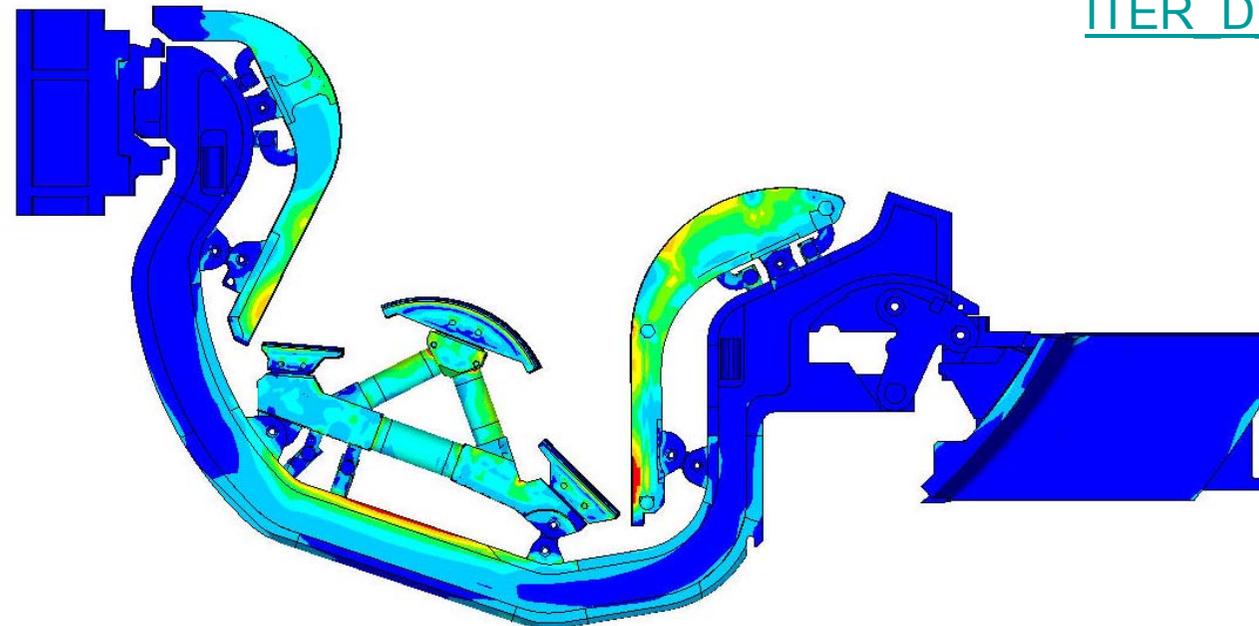
	Individual events in ITER tokamak			Additional loads specific to divertor	Category	Number of events ⁽¹⁾
	Seism	Plasma ⁽³⁾	Magnet			
1		Testing regime		DW, Hydr. test pressure,	Test	1
2		Baking regime ⁽²⁾		Preload, DW, CP, TH	I	200 at 240 C 4.4 MPa 200 at 350 C at 1 MPa
3		Normal operation		Preload, DW, CP, TH	I	Only for thermal loads: 5000 for PFCs and CB @ 10 MW/m ² 300 for PFCs and CB @ 20 MW/m ² 30,000 for rails
4		SDVDE-II 50-100 ms		Preload, DW, CP, TH	II	150
5		FDVDE-II 36 ms		Preload, DW, CP, TH	II	150
6		MD-I 50 ms	MFD-II	Preload, DW, CP, TH	II	3000
7	SL-1 ⁽³⁾		MFD-II	Preload, DW, CP, TH	II	1
8		SDVDE-III (>200ms)		Preload, DW, CP, TH	III	1
9		FDVDE-III 36 ms		Preload, DW, CP, TH	III	1
10	SL-1 ⁽³⁾	SDVDE-II 50-100 ms	MFD-II	Preload, DW, CP, TH	III	1
11	SL-1 ⁽³⁾	FDVDE-II 36 ms	MFD-II	Preload, DW, CP, TH	III	1
12	SL-2 ⁽³⁾			Preload, DW, CP, TH	IV	1
13		SDVDE-IV slow-fast		Preload, DW, CP, TH	IV	1
14		“Rotating Asymmetric VDEs”		Preload, DW, CP, TH	IV	1
15	SL-2 ⁽³⁾	Baking regime		Preload, DW, CP, TH	IV	1
16	SL-2 ⁽³⁾	Maintenance		DW	IV	1

Load Specification for the ITER Divertor System (C9RF33)

Design Supporting Analysis Results

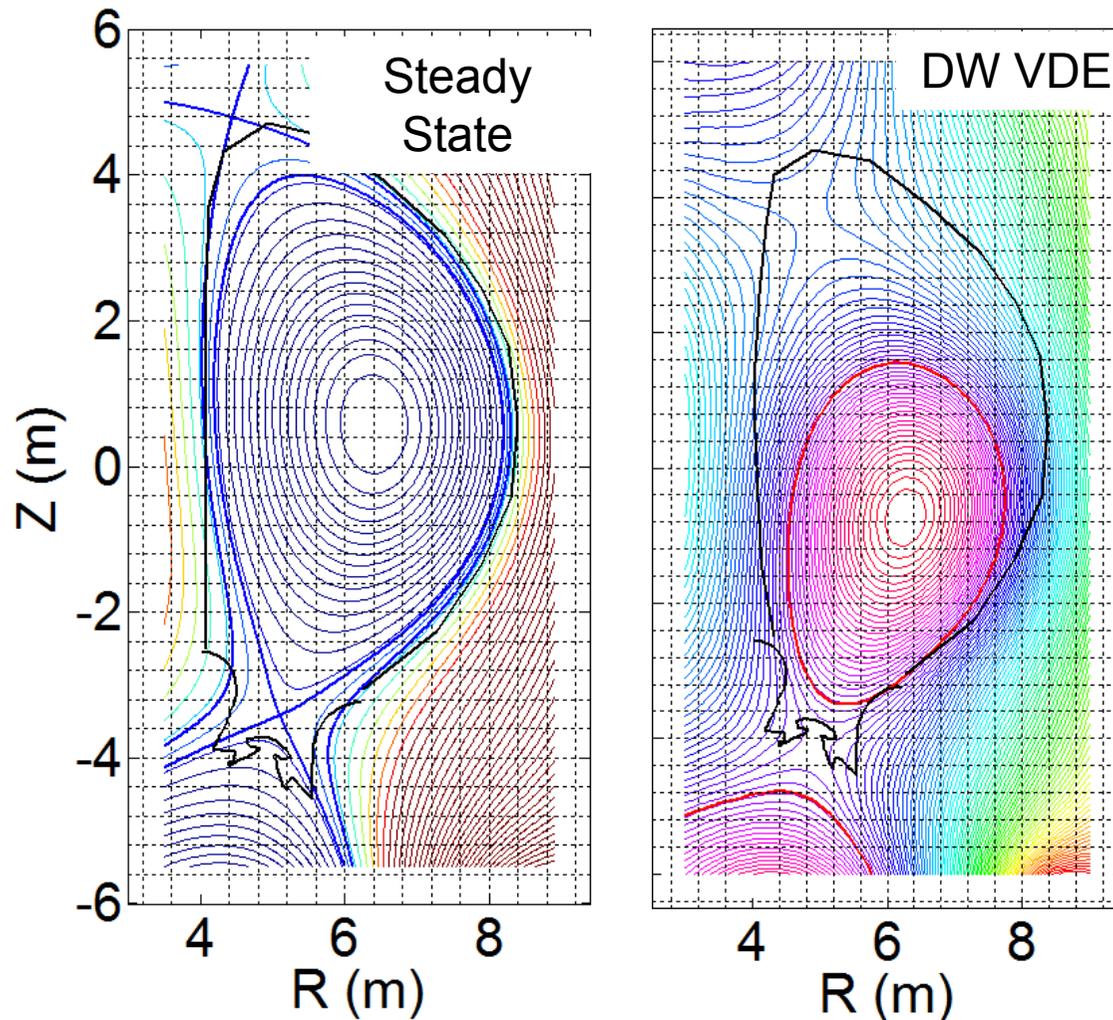
Stress intensity (MPa) at 2nd load combination: CB preload + DW+ CP + Temperature

ITER D HR2ZCU



- Primary stresses are within allowable limits for the analysed load cases (DW, Pressure test, Coolant pressure, EML)
- Cyclic strength criteria (no ratcheting) are satisfied for the SSS of the PFCs, Dome PFUs and CB.

Heat Load distribution study – PFC level



Input:

- Plasma configurations
- Heat load specification
- Max misalignment at gap
- Plasma-facing surface envelop

Tool:

PFCFLUX – 3D field line tracing code

Aim:

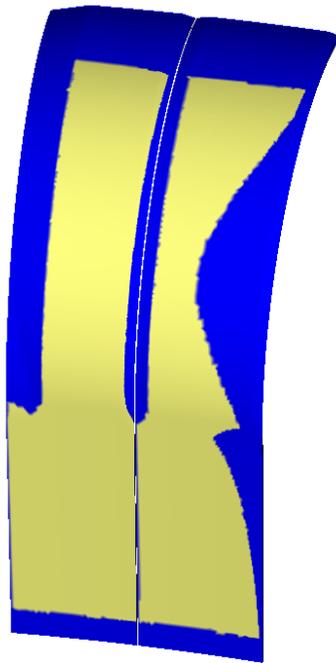
Validate full edge shadowing during Steady State and VDEs

Key component: OVT

Heat Load Distribution Analysis Results

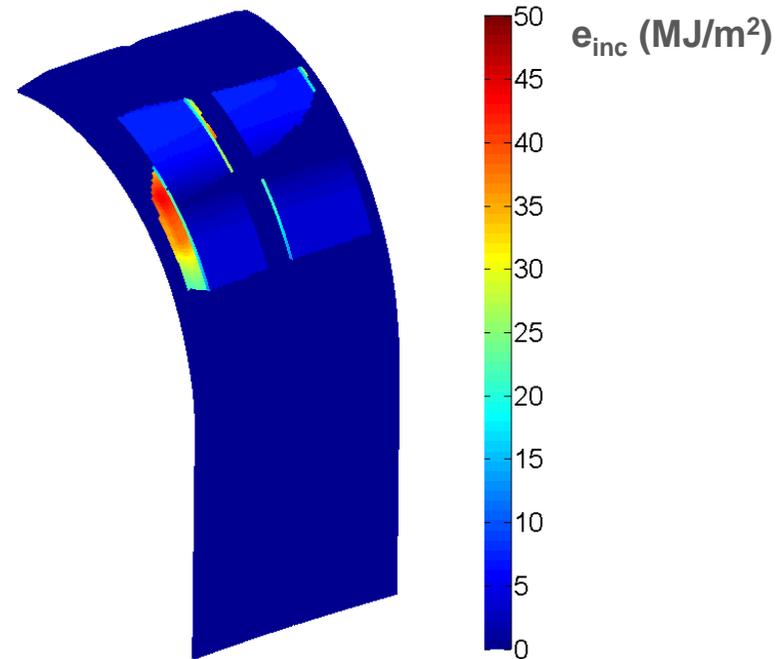
- Examin 5 (I_p , B_T) steady-states
→ **No leading edges**
- Examine Analysis of ~75 DINA time sequences → **no leading edges**

15MA, 5.3T



Wetted area at OVT surface
With worst misalignment

'DW VDE, init li = 0.6, 675 ms'

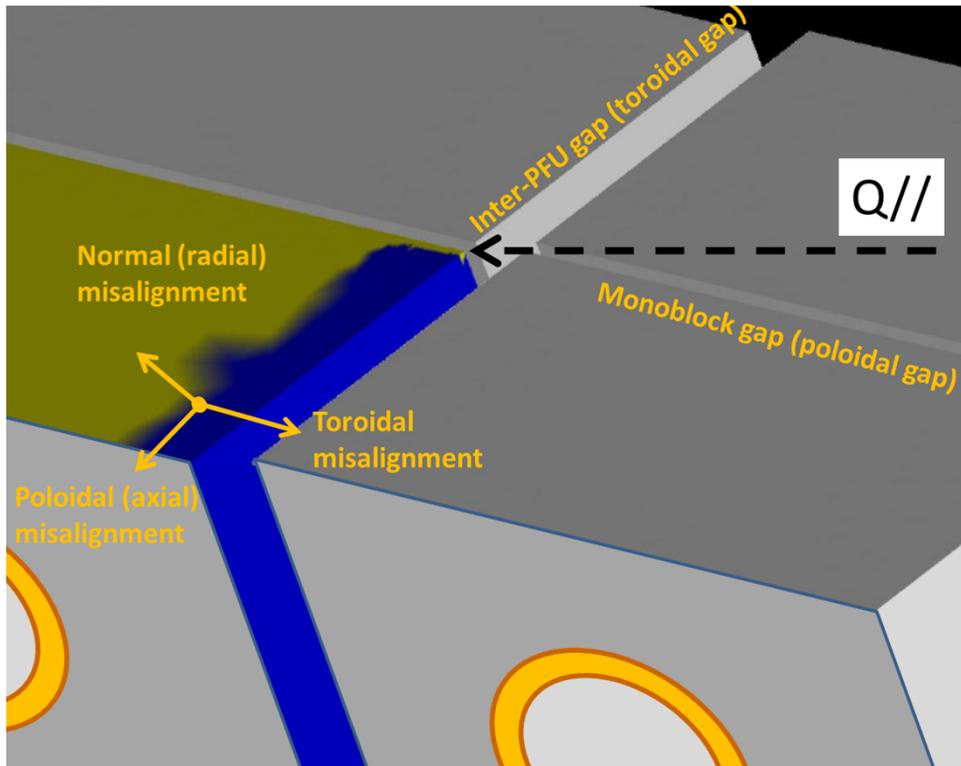


Energy density at OVT surface
With worst misalignment

- Demonstrates OVT shaping design could avoid leading edges

Heat Load distribution study – monoblock level

Monoblock (axial 12 mm; toroidal 28 mm) edges could be exposed to **flux tubes penetrating through the monoblock gaps** (nominal width 0.5 mm).



Input:

- Plasma configurations
- Heat load specification
- Max misalignment at gap
- Monoblock geometry

Tool:

1. PFCFLUX:

Field tracing analysis (optical)

2. Monte Carlo test particle simulation:

Ions with random perpendicular velocities (Maxwellian distribution) in magnetic field

Aim:

Validate full edge shadowing at HHF area at monoblock level

Under final tuning: double chamfer

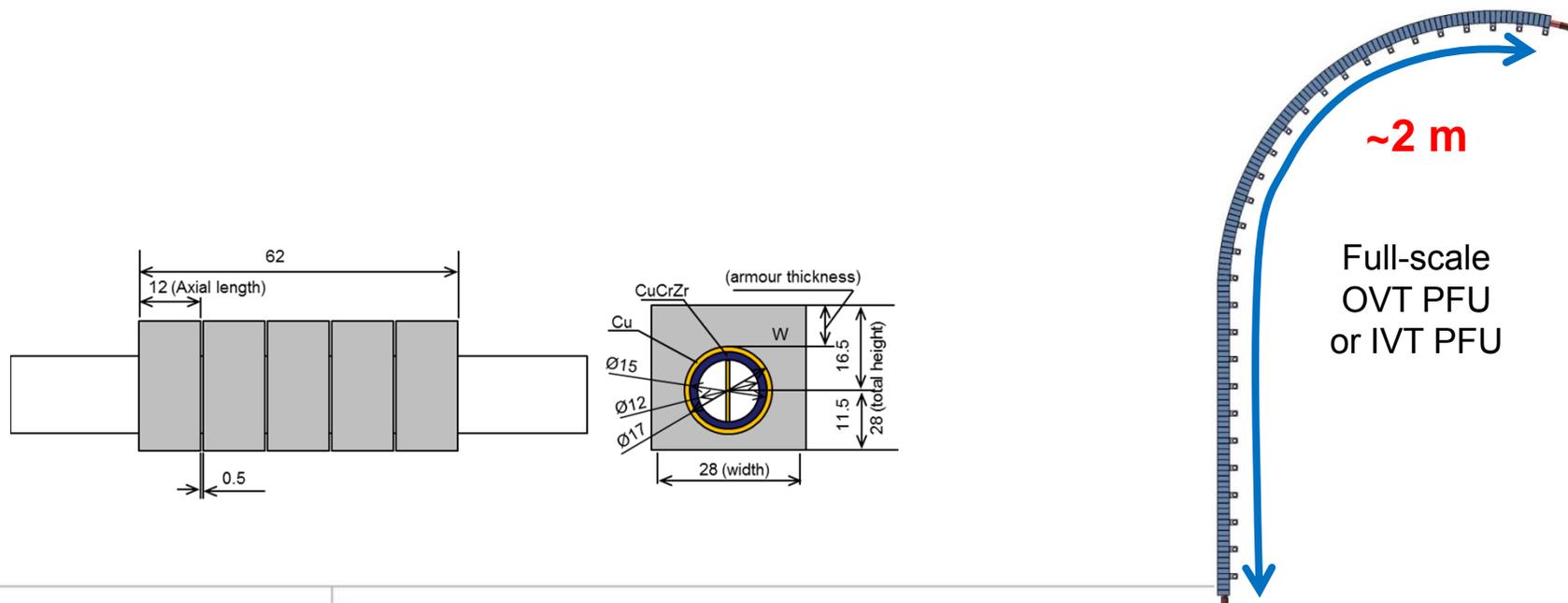
Outline

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Full-W Divertor Qualification Program

2 steps in the program

- (1) Technology Development and Validation** : Demonstration of the *fitness-for-purpose* of the proposed technology, full-W small-scale mock-ups manufacturing and High Heat Flux testing
- (2) Full-scale demonstration** : Demonstration of the technology via full-scale-prototype PFU manufacturing and testing in IDTF; Compliance with IO procurement quality requirement



1st step: Technology Development and Validation

- **PFU attachment joint**

(1) **Uniaxial tensile test** at RT (at least 5 samples; Load speed 20-60 N/s)

Acceptance Criteria: >8 kN for OVT and >10 kN for IVT (attachment/5monoblocks)

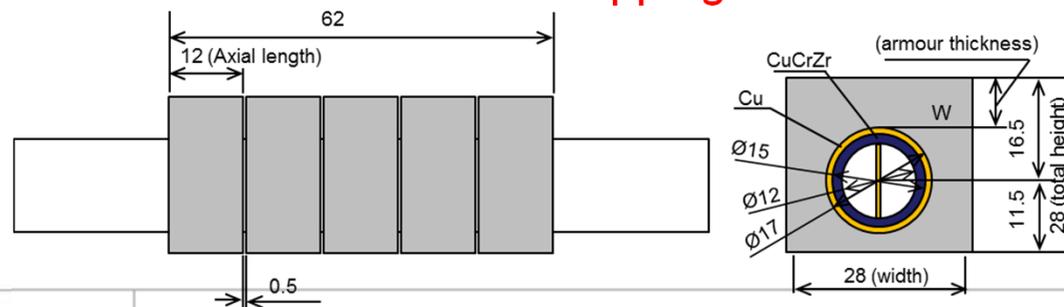
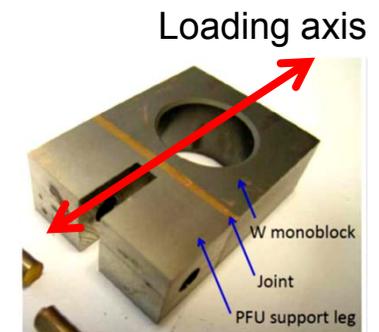
(2) **Cyclic zero-pull fatigue test** at RT cycle number 15k cycles (<1 Hz) 0-8 kN (0-10kN) OVT (IVT) PFU leg (attachment/5monoblocks)

Acceptance Criteria: deformation along the loading axis < 0.3 mm

- **W monoblock armor to heat sink joint**

HHF test 5000 cycles at 10 MW/m² and 300 cycles at 20 MW/m²

Acceptance Criteria: No trace of substantial melting by Visual Inspection / No water leak / No detachment of any armour block / No appearance of any “hot spot” during fatigue cycling / no variation of max T_{surf} (°C) exceeding 20% increase between initial and final thermal mapping



2nd step: Full-scale demonstration

- **Tube to tube joint qualification**

(1) **Welding qualification test** in accordance to EN ISO 15614-1

Acceptance Criteria: Quality class B as defined in EN ISO 5817 or EN ISO 13919-1, and ITER Vacuum Handbook Attachment-1

(2) **He leak test after rotary bending fatigue test** 0.1% strain, 10k cycles (<1Hz) at RT

Acceptance Criteria: He leak rate $\leq 10^{-10}$ Pa m³/s

(3) **Tensile test** at 150°C

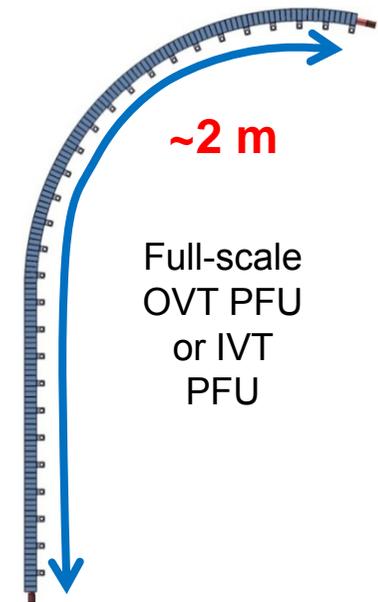
Acceptance Criteria: > 200 MPa

- **PFU W monoblock armor to heat sink joint**

- **HHF test 5000 cycles at 10 MW/m² and 300 cycles at 20 MW/m² at straight part**

- **HHF test 5000 cycles at 5 MW/m² at curved part**

Acceptance Criteria: No trace of substantial melting by Visual Inspection / No water leak / No detachment of any armour block / No appearance of any “hot spot” during fatigue cycling / no variation of max T_{surf} (°C) exceeding 20% increase between initial and final thermal mapping

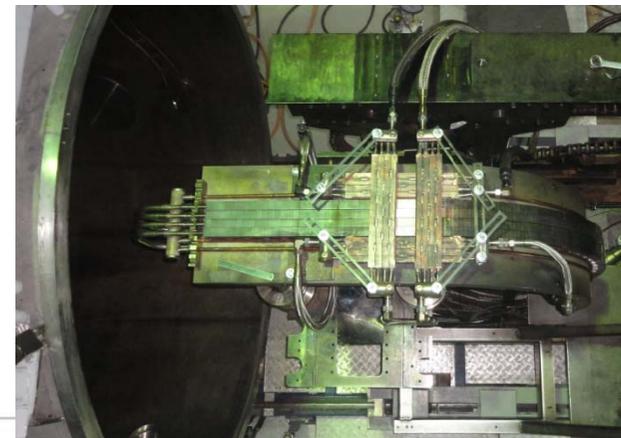
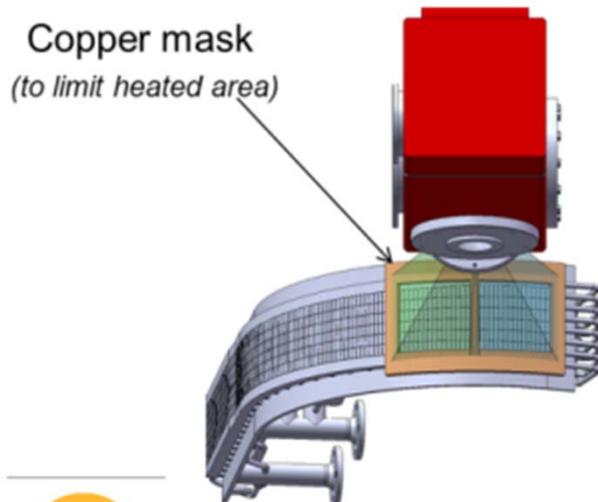
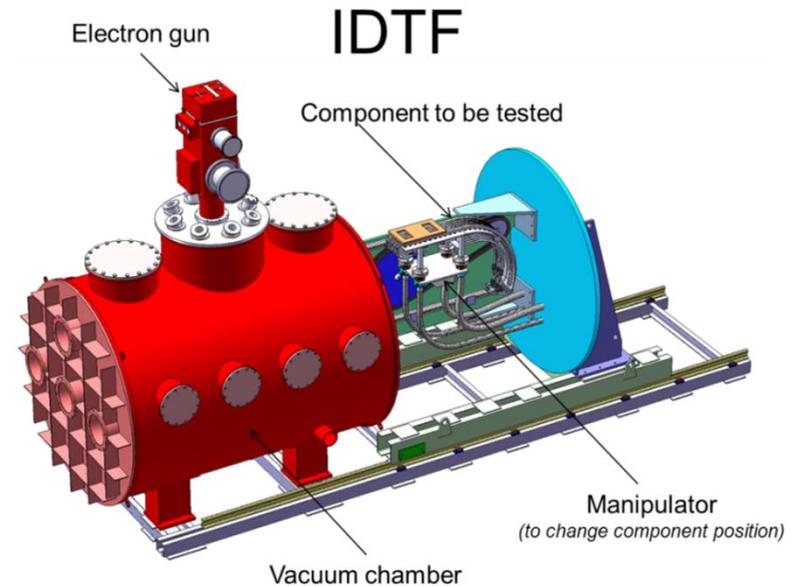


- **Compliance with ITER Procurement Quality Requirements**

ITER Divertor Test Facility (IDTF)

IDTF that commissioned in frame of Divertor PA

- Built within Procurement Arrangement 17P2D
- Location: Efremov Institute, St-Petersburg, RF
- Electron beam test facility
- Maximum electron beam power: 800 kW
- Maximum accelerating voltage: 60kV
- Cooling water parameters are ITER divertor relevant
- Dedicated system of diagnostics



Task Agreements to support technology R&D

- **Objectives:**

- Deliver results of **technology validation timely for the decision of the armour material (end 2013)**
- Support **demonstration by the full-scale prototypes** activities

- **3 TAs with DAs**

- With JA DA: for the manufacturing of OVT small-scale mock-ups and full-scale prototype PFUs
- With EU DA: for the manufacturing of IVT small-scale mock-ups (full-W full-scale PFU manufacturing already planned in the PA for IVT)
- With RF DA: for the HHF testing of the above components at the ITER Divertor Test Facility (IDTF)

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EU HHF Test Results 2009-2011

HHF tests were performed on the FE200 facility at AREVA. Tungsten monoblock mock-ups armouring CuCrZr cooling pipes were successfully tested up to 15 MW/m² for 1000 cycles and 20 MW/m² for 300 cycles [1].

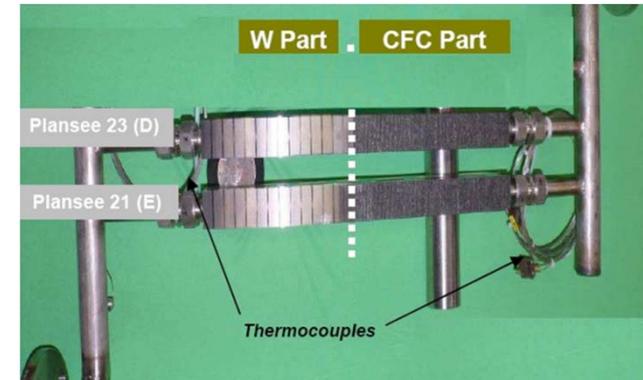
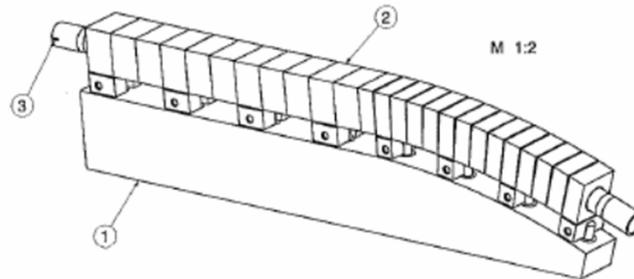


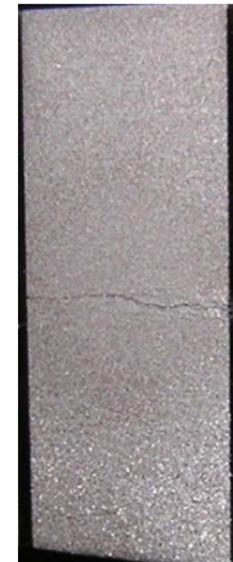
Table summarizes the main results on the tested tungsten mock-ups [2]

1000 cycles at 10 MW/m ²	1000 cycles at 15 MW/m ²	300 cycles at 20 MW/m ²
No significant visible effect	Surface modification but no melting trace	Self-castellation ; No debonding of tile ; no substantial melting

Results fulfil the IO acceptance criteria, and indicate that W monoblock technology is acceptable for the requirements of the full-W vertical target

[1] P. Gavila et al, *Fus. Eng. & Des.* 86 (2011) 1652-1655

[2] P. Lorenzetto et al, 24th IAEA-FEC 2012

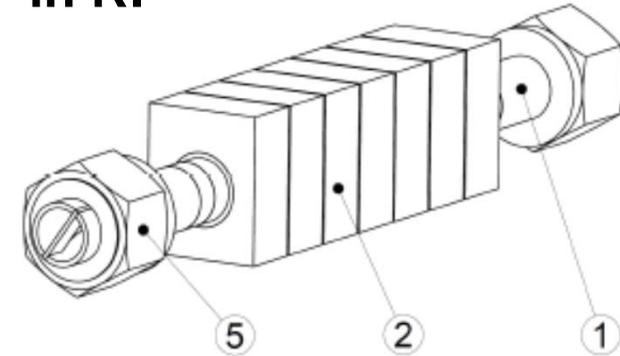


EU HHF test results in 2013

EU DA campaign: on 12 mock-ups in IDTF in RF

HHF Testing program:

- step 1 : 5000 cycles at 10 MW/m²
- step 2 : 300 (+700 cycles) at 20 MW/m²
- step 3 : critical heat flux



HHF results @ 20MW/m² obtained on first set of 6 mock-ups.

- No traces of melting on the loaded surface
- Cracking development

Second set of HHF testing program with 6mm of W thickness was recently stopped.

Ansaldo 20MW/m² after 75 cycles

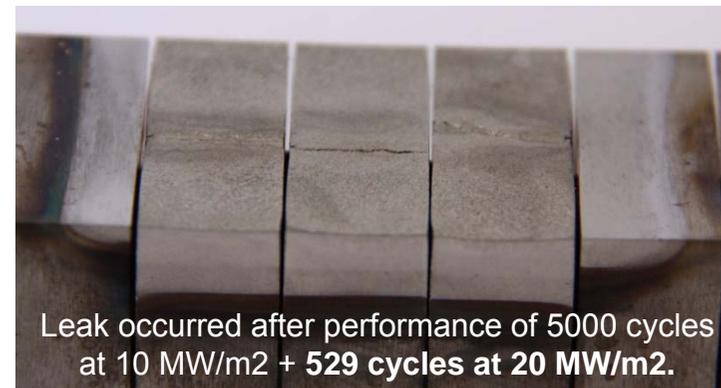


with 6 mm of W thickness

Plansee 20MW/m² after 75 cycles



with 7.5 mm of W thickness



Leak occurred after performance of 5000 cycles at 10 MW/m² + 529 cycles at 20 MW/m².

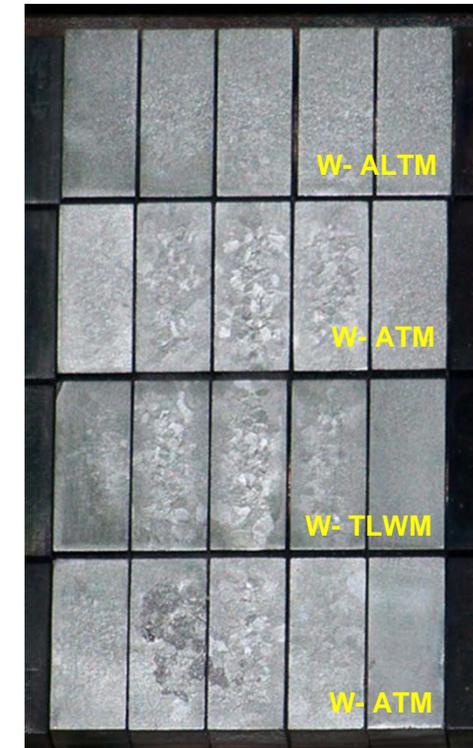
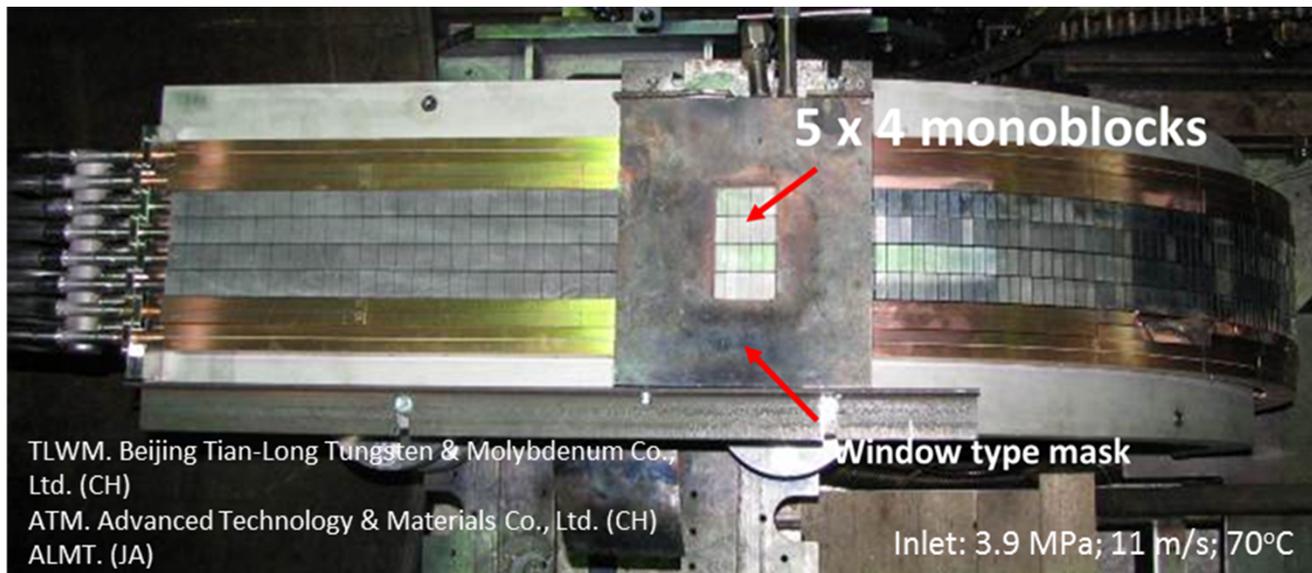
Self-castellation was observed

JA HHF results in 2012

JA DA campaign: OVT CFC/W Full-Scale PFUs

Straight W part of PFUs subjected to the HHF tests -- 5000 cycles at 10 MW/m² and 1000 cycles at 20 MW/m²

20 monoblocks of 12mm (axial) x 28mm (poloidal) x 7.5 mm (W thickness at the top of the tube).

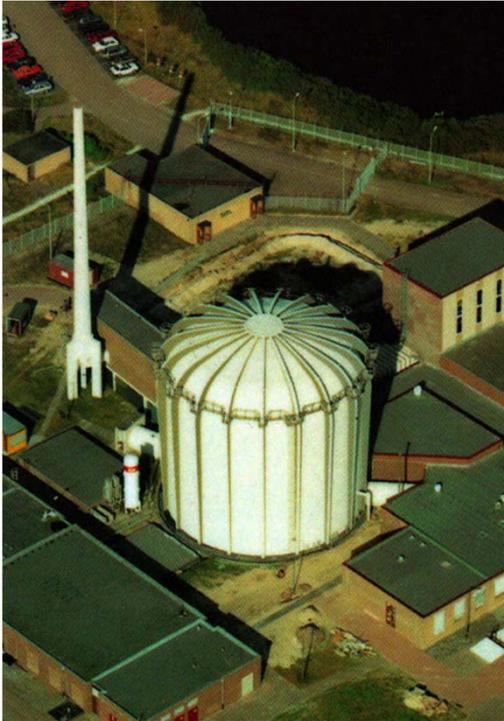


Results fulfil the IO acceptance criteria, and indicate that W monoblock technology is acceptable for the requirements of the full-W vertical target

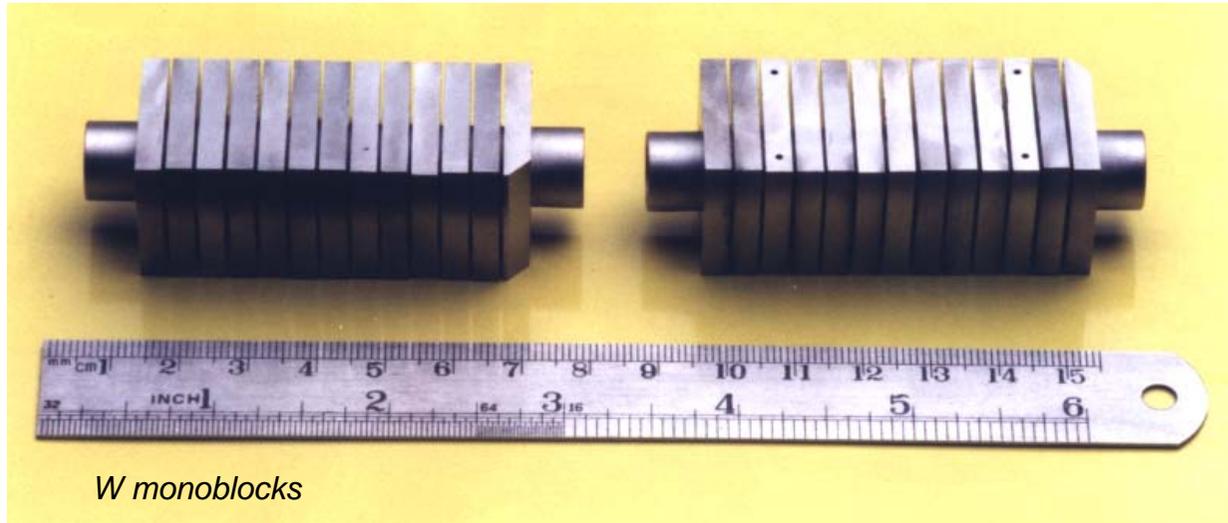
Small scale mockups will be tested in IDFT 24-26 Sep 2013

Effects of Irradiation on Performance

The effects of irradiation on the performance of the W monoblock have been assessed by experiments – PARIDE 3 and PARIDE 4 [4].



High Flux Reactor
Petten, Netherlands



W monoblocks

Neutron-Irradiation campaign:

PARIDE 3: 0.1 dpa at 200 °C // PARIDE 4: 0.6 dpa at 200 °C

Irradiated W mock-ups (0.6 dpa at 200°C) sustained thermal fatigue testing at 18 MW/m² for 1000 cycles

Post irradiation testing of samples from the irradiation experiments PARIDE 3 and PARIDE 4, M. Roedig et al., JNM 329–333 (2004) 766–770

Outline

1. Design constrain/input
2. Detailed divertor PFC Design
3. Design Validation
4. Technology R&D requirements
5. Progress of technology R&D in EU and JA
- 6. Conclusion/Schedule**

Schedule for full-W Divertor Decision

- **Final Design Review** of Tungsten Divertor (26-28 June 2013)
 - ✓ Full-W Divertor design
 - ✓ Full-W Divertor technology qualification programme
- **Physics Assessment**
 - ✓ Report from ITPA Topical Groups to STAC-14 (May 2013) giving a physics/operational opinion on a full-W divertor start for ITER
 - ✓ JET misaligned lamella melt experiment: summer 2013
- **STAC-15 (Oct 2013) to take note** of the Design and Physics outcome and provide recommendation
- **ITER Council-13 (Nov 2013) to endorse the STAC/ MAC recommendation on this topic**
- **Implementation of the decision into the baseline** via a PCR (end-2013, *SMP.0116.001032 milestone*) if selected

Thank you very much for your attention